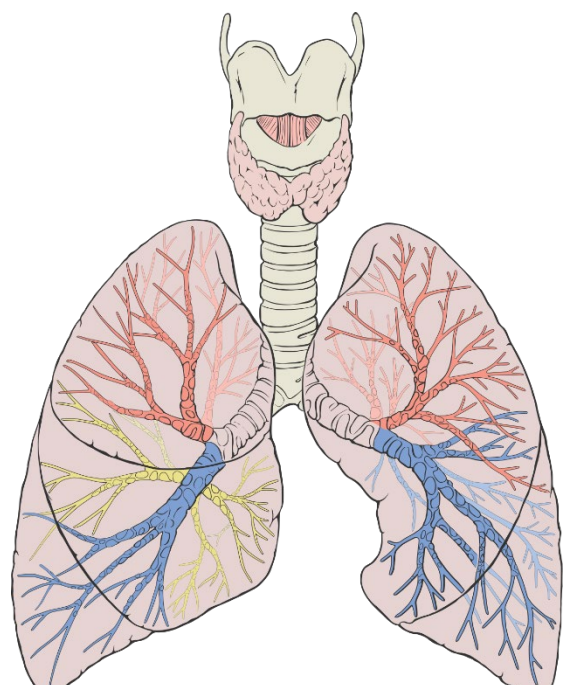


## Chapter 8

### Viscous Flow in Pipes

### Laminar and Turbulent Flows





**LAMINAR VS. TURBULENT FLOW**

# Objectives

- Identify and explain various characteristics of pipe flow.
- Understand and discuss main properties of laminar and turbulent flow.
- Calculate losses in straight pipes and components and determine **pressure drops** and require **pumping power to overcome pressure drop and losses**.
- Be able to use Moody diagram and Haaland equation to iteratively solve for FLOW RATE and Diameters.

# Energy Equation

## Real Systems—SINGLE IN/OUT

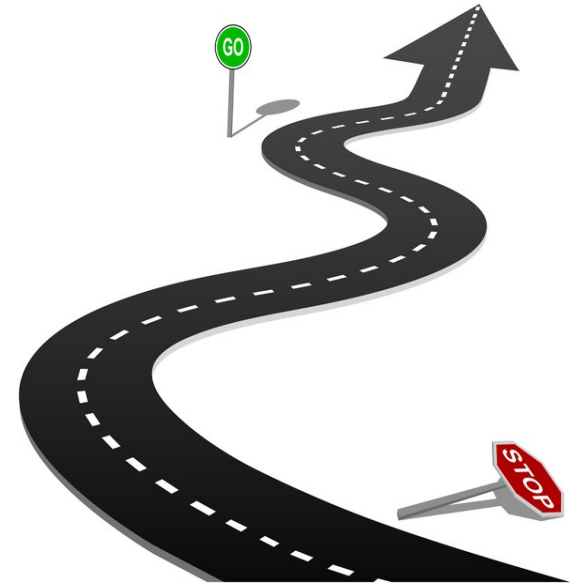
$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 + h_{p_{IDEAL}} = h_{T_{IDEAL}} + \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_q + h_{L_{major}} + h_{L_{minor}}$$

→ All terms "ft" or "m"

$h_p \equiv IDEAL PUMP POWER$

$h_T \equiv IDEAL TURBINE POWER$

$$h_q \equiv \frac{u_2 - u_1 - \frac{\dot{Q}}{\dot{m}}}{g} \rightarrow THERMAL LOSS$$





# Energy Equation

## Real Systems—MULTIPLE IN/OUT

$$\sum_{in} \dot{m}g \left( \frac{P_{in}}{\gamma} + \frac{V_{in}^2}{2g} + z_{in} \right) + \dot{m}g(h_{p_{IDEAL}}) = \dot{m}g(h_{T_{IDEAL}}) + \sum_{out} \dot{m}g \left( \frac{P_{out}}{\gamma} + \frac{V_{out}^2}{2g} + z_{out} \right) + \dot{m}g(h_{TOTAL})$$

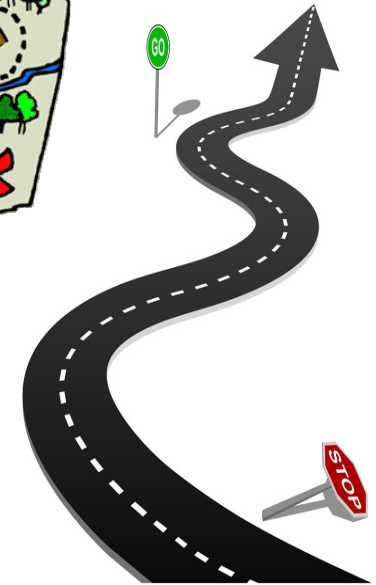
$$\dot{m}g(h) = \gamma Q(h) \rightarrow \text{WATTS, or, } \frac{\text{ft} - \text{lbf}}{\text{s}}$$

$$h_p \equiv \text{IDEAL PUMP POWER HEAD (m or ft)}$$

$$h_T \equiv \text{IDEAL TURBINE POWER HEAD (m or ft)}$$

$$h_{TOTAL} = h_q + h_{L_{major}} + h_{L_{minor}} \rightarrow \text{TOTAL POWER FLOW LOSS (m or ft)}$$

$$h_q \equiv \frac{(u_2 - u_1) \left[ \frac{J}{kg} \right] - \frac{\dot{Q}}{\dot{m}} \left[ \frac{J}{kg} \right]}{g} \rightarrow \text{THERMAL LOSS}$$



# Pump and Turbine Power & Efficiency

$$W_{P_{ACTUAL}} = \frac{\gamma Q h_{P_{IDEAL}}}{\eta_p} = \frac{Q \Delta P}{\eta_p} \rightarrow \text{PUMP}$$

$$W_{T_{ACTUAL}} = \gamma Q h_{T_{IDEAL}} \eta_t \rightarrow \text{TURBINE}$$

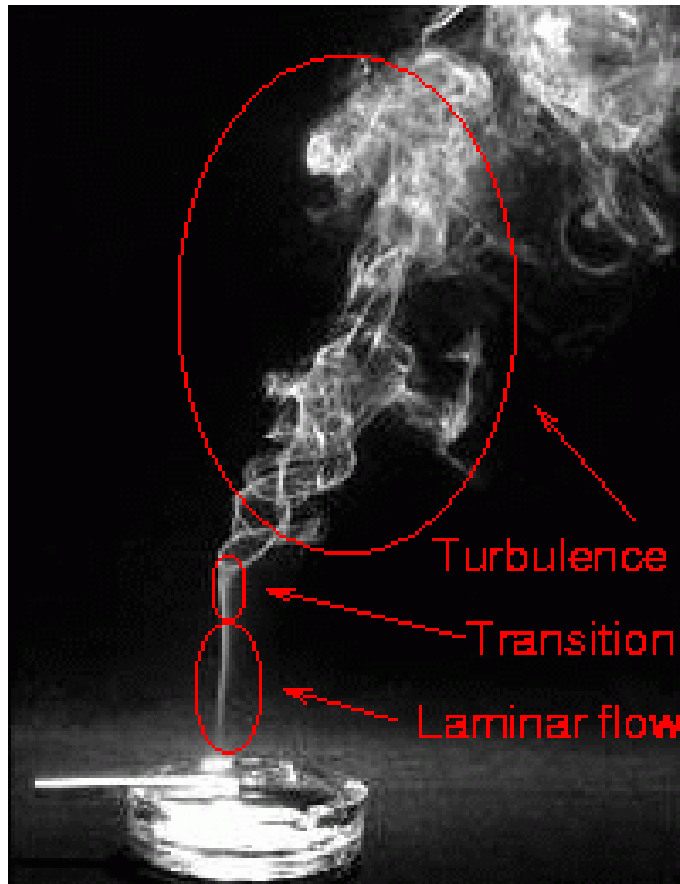


$$\eta_p \equiv \text{pump efficiency} = \frac{W_{ideal}}{W_{actual}} = \frac{W_{actual} - \text{LOSS}}{W_{actual}}$$

$$\eta_t \equiv \text{turbine efficiency} = \frac{W_{actual}}{W_{ideal}} = \frac{W_{actual}}{W_{actual} + \text{LOSS}}$$

# Flow Visualization

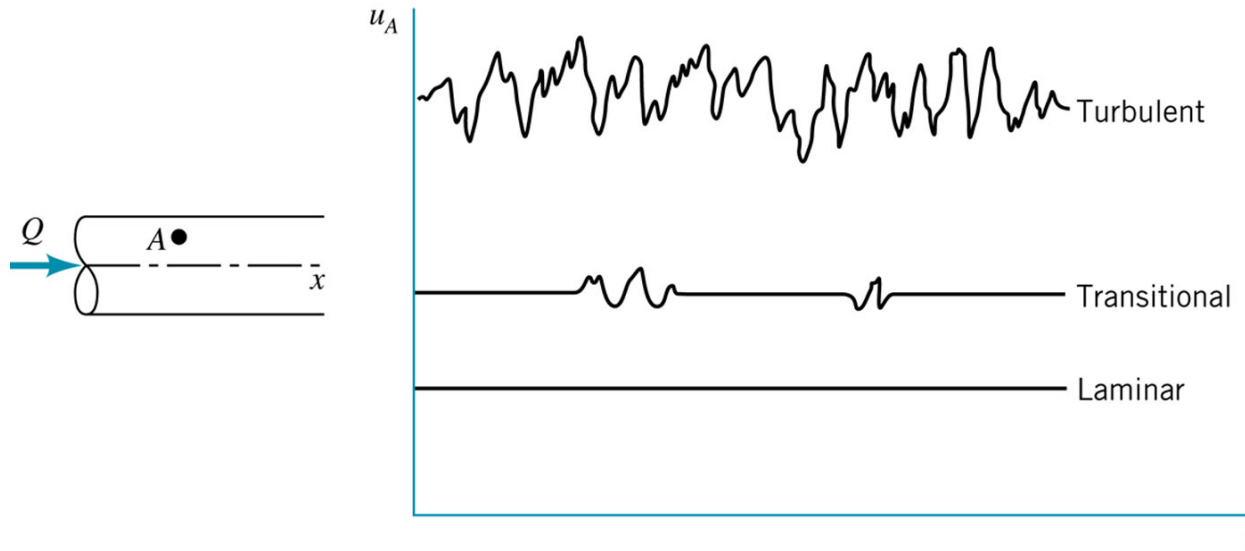
- Reynolds Experiment (Pipe Flow)



<https://www.youtube.com/watch?v=9A-uUG0WR0w>

Fluid Dynamic Instabilities!  
PLEASE DO NOT SMOKE !!!

# Laminar or Turbulent Flow



- **Reynolds Number**

$$\text{Re}_D = \frac{\rho V D_H}{\mu} = \frac{V D_H}{\nu}$$

**Laminar Flow:**  $\text{Re}_{D_H} \leq 2100$

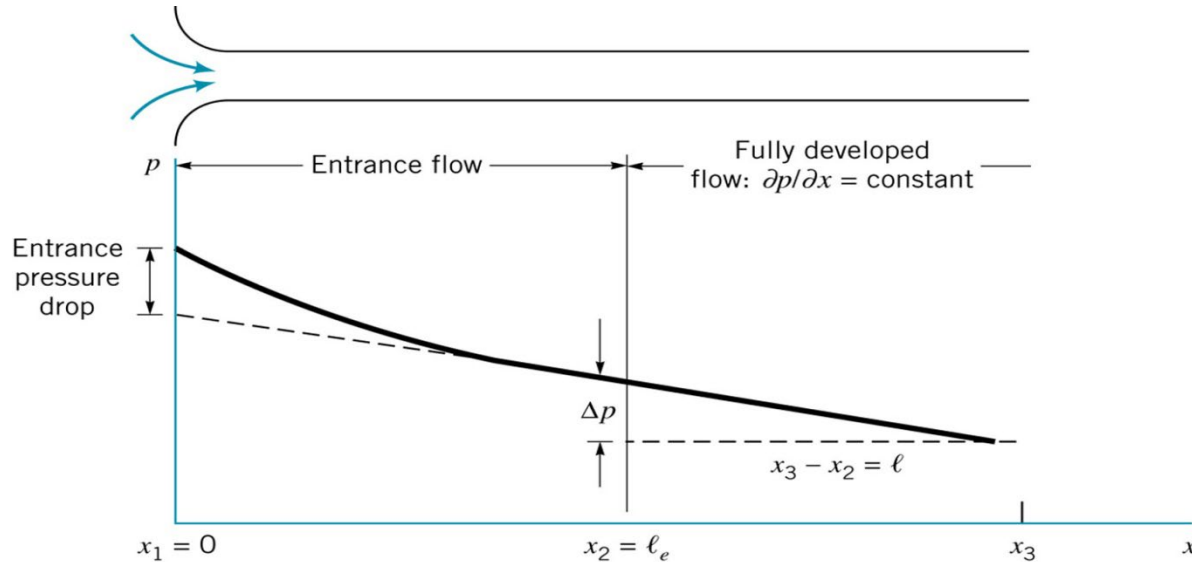
**Transitional Flow:**  $2100 < \text{Re}_{D_H} \leq 4000$

**Turbulent Flow:**  $\text{Re}_{D_H} > 4000$



# Entrance Length, Fully Developed Flow

## What Causes fluid to flow through the pipe?

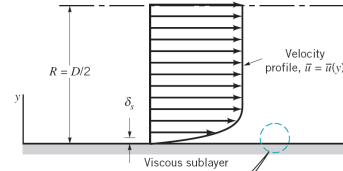


- For horizontal pipe flow, gravity has no effect except for a hydrostatic pressure variation across the pipe.
- The pressure difference,  $\Delta p = p_1 - p_2$  forces the fluid through the pipe.
- Pressure force is needed to overcome the viscous forces generated.
- Nature of the pipe flow is dependent on whether the flow is laminar or turbulent.

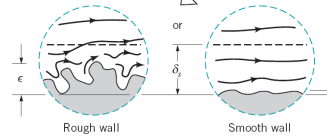
# Friction factor & head loss

- **Friction factor for laminar/turbulent pipe flow:**

$$f_{LAM} = \frac{8\tau_w}{\rho V^2} = \frac{64}{Re_{D_H}}$$



$$f_{TURB} = \phi(Re_{D_H}, \epsilon/D_H)$$



$\epsilon/D_H \equiv$  Relative Roughness (pipe wall interior)

- **Pressure Drop & Head Loss:**

$$\Delta p = f \left( \frac{l}{D_H} \right) \frac{\rho V^2}{2} \left( \text{pressure drop} - Pa; \frac{lbf}{ft^2} \right)$$

$$\Rightarrow h_L = \frac{\Delta p}{\gamma} = f \left( \frac{l}{D_H} \right) \frac{V^2}{2g} \left( \text{energy loss} - m; ft \right)$$

**Hydraulic Diameter:**  $D_H = \frac{4A_c}{P}$ ,  $A_c$  = CROSS-SECTION area;  $P$  = Wetted Perimeter

(non-circular pipe)

# Friction factor & head loss

**Example Problem:** A fluid flows through a 0.1in diameter pipe. When the Reynolds number is 1500, the head loss over a 20ft long pipe is 64ft. Determine the fluid velocity.

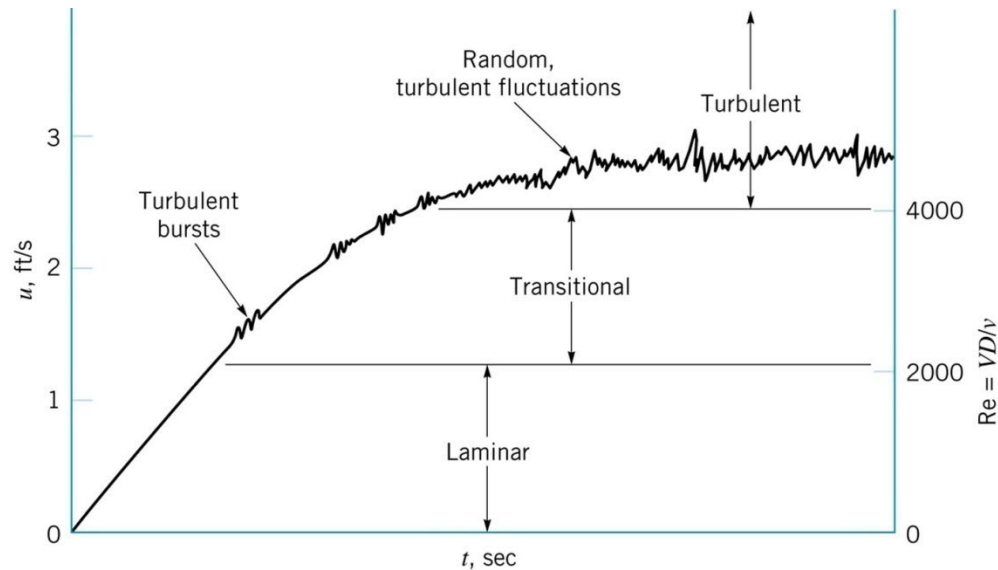
**Solution:** Since Reynolds number = 1500 < 2100. The flow is Laminar. Hence

$$f = \frac{64}{\text{Re}_D} = \frac{64}{1500}$$
$$\Rightarrow f = 0.043$$

**Now**

$$h_L = f \left( \frac{l}{D} \right) \frac{V^2}{2g}$$
$$\Rightarrow 64 \text{ ft} = 0.043 \left( \frac{20 \text{ ft}}{0.1 \text{ in} / 12 \text{ in} / \text{ft}} \right) \frac{V^2}{2(32.2 \text{ ft} / \text{s}^2)}$$
$$\Rightarrow V = 6.32 \text{ ft} / \text{s}$$

# Fully Developed Turbulent Flow



- **Turbulent is a very complex flow pattern**
- **Mixing processes (heat, mass transfer) are considerably enhanced due to the macroscopic scale of randomness.**
- **Without turbulence it would be virtually impossible to carry out life as we now know it.**
- **In some situations turbulent flow is desirable and in others they are a disadvantage.**

$$\left[ \frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 + \frac{h_{P_{IDEAL}}}{\eta_p} = \eta_t h_{T_{IDEAL}} + \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_q + h_L \right]$$

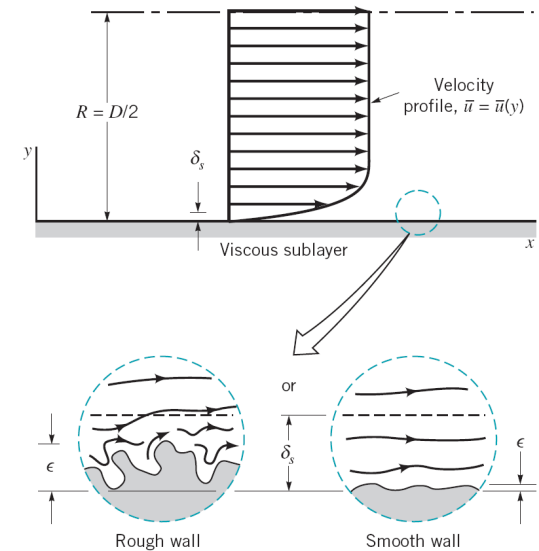
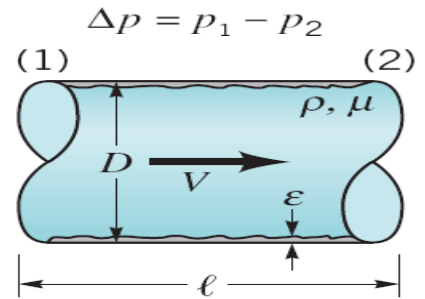
$$h_L = h_{L_{major}} + h_{L_{minor}}$$

$$h_q \equiv \frac{u_2 - u_1 - \frac{\dot{Q}}{\dot{m}}}{g}$$

- **Most turbulent pipe flow information is based on experimental data.**
- It is often necessary to **determine the head loss** that occurs in a pipe flow
- The **overall head loss for the pipe system** consists of the **head loss due to viscous effects** in the straight pipes, termed the **major loss** and the **head loss in the various pipe components** termed the **minor loss.**

# Major Losses

- **Turbulent pipe flow properties depend on the fluid density and the pipe roughness.**
- For turbulent flow the **pressure drop** is expected to be a function of the wall roughness,  $\epsilon$ .
- The **relative roughness** ( $\epsilon/D$ ) for typical constant diameter pipes is between 0 and 0.05.



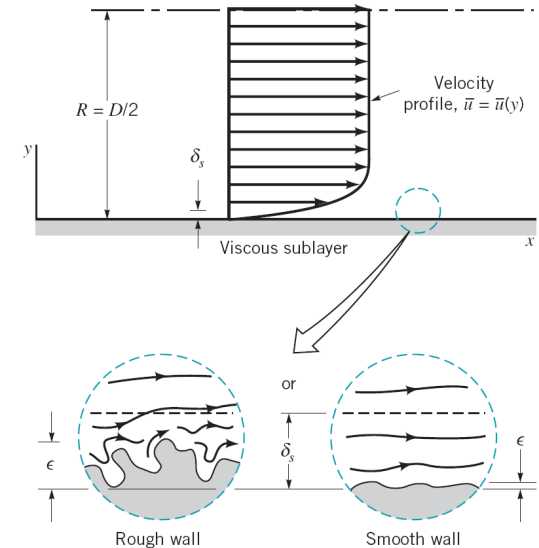
$$\frac{\delta_s}{D} \ll 1$$

$$0 \leq \epsilon / D \leq 0.05$$



# Friction factor for Turbulent flow

- Turbulent flow, the functional dependence of the friction factor on the Reynolds number and the relative roughness is a rather complex one that cannot, as yet be obtained from a theoretical analysis.



$$h_{L,major} = f \frac{\ell}{D} \frac{V^2}{2g}$$

$$f_{TURB} = \phi(\text{Re}_D, \epsilon/D)$$

■ TABLE 8.1

Equivalent Roughness for New Pipes [From Moody (Ref. 7) and Colebrook (Ref. 8)]

Pipe	Equivalent Roughness, $\epsilon$	
	Feet	Millimeters
Riveted steel	0.003–0.03	0.9–9.0
Concrete	0.001–0.01	0.3–3.0
Wood stave	0.0006–0.003	0.18–0.9
Cast iron	0.00085	0.26
Galvanized iron	0.0005	0.15
Commercial steel or wrought iron	0.00015	0.045
Drawn tubing	0.000005	0.0015
Plastic, glass	0.0 (smooth)	0.0 (smooth)

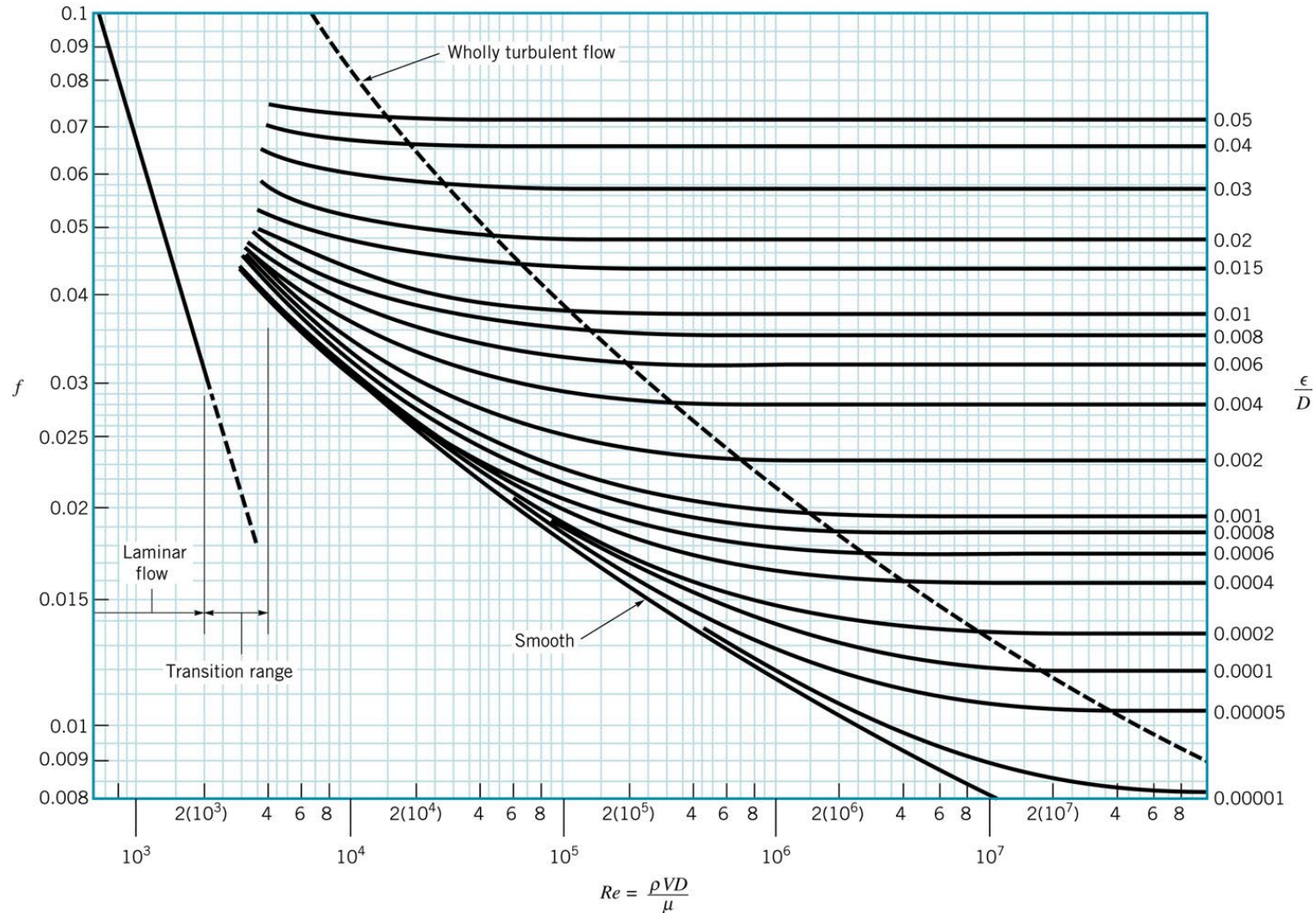
# Moody diagram

Haaland EQN. formula for turbulent flow

$$f = \frac{64}{Re_D}; \text{Laminar Flow}$$

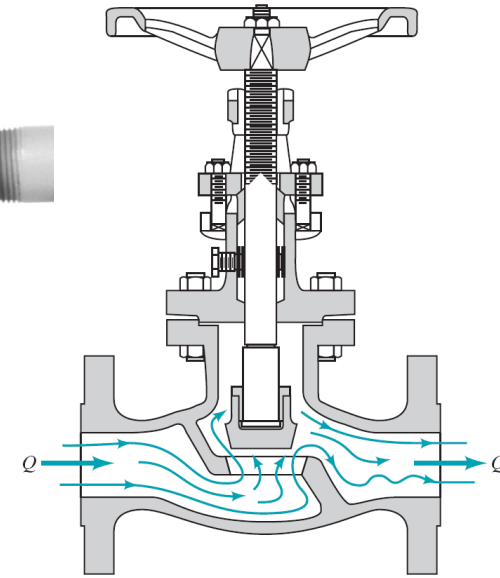
Wall roughness & friction factor

$$\frac{1}{\sqrt{f}} = -1.8 \log_{10} \left( \left( \frac{\epsilon / D}{3.7} \right)^{1.11} + \frac{6.9}{Re} \right)$$



# Minor Losses

- Most pipe systems, consist of components (valves, bends, tees and the like) that adds to the overall head loss of the system.
- The head losses from these components are generally termed minor losses.
- Loss coefficient  $K_L$  is used for these head losses or pressure drops



$$\sum K_L = \frac{h_{L \text{ minor}}}{(V^2/2g)} = \frac{\Delta p}{\frac{1}{2} \rho V^2}$$



$$\Delta p = (\sum k_L) \frac{1}{2} \rho V^2$$

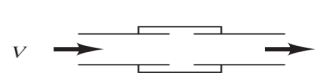
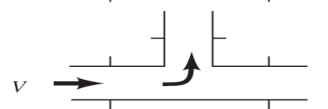
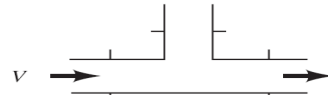
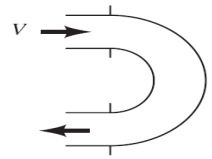
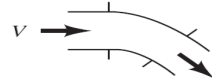
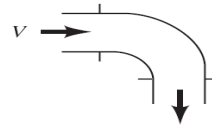
$$\text{or } h_{L \text{ minor}} = (\sum k_L) \frac{V^2}{2g}$$

# Loss coefficient for piping components

■ TABLE 8.2

Loss Coefficients for Pipe Components ( $h_L = K_L \frac{V^2}{2g}$ ) (Data from Refs. 5, 10, 27)

Component	$K_L$
<b>a. Elbows</b>	
Regular 90°, flanged	0.3
Regular 90°, threaded	1.5
Long radius 90°, flanged	0.2
Long radius 90°, threaded	0.7
Long radius 45°, flanged	0.2
Regular 45°, threaded	0.4
<b>b. 180° return bends</b>	
180° return bend, flanged	0.2
180° return bend, threaded	1.5
<b>c. Tees</b>	
Line flow, flanged	0.2
Line flow, threaded	0.9
Branch flow, flanged	1.0
Branch flow, threaded	2.0
<b>d. Union, threaded</b>	
	0.08
<b>*e. Valves</b>	
Globe, fully open	10
Angle, fully open	2
Gate, fully open	0.15
Gate, $\frac{1}{4}$ closed	0.26
Gate, $\frac{1}{2}$ closed	2.1
Gate, $\frac{3}{4}$ closed	17
Swing check, forward flow	2
Swing check, backward flow	$\infty$
Ball valve, fully open	0.05
Ball valve, $\frac{1}{3}$ closed	5.5
Ball valve, $\frac{2}{3}$ closed	210



$$K_{L_{inlet}} = 0.5$$

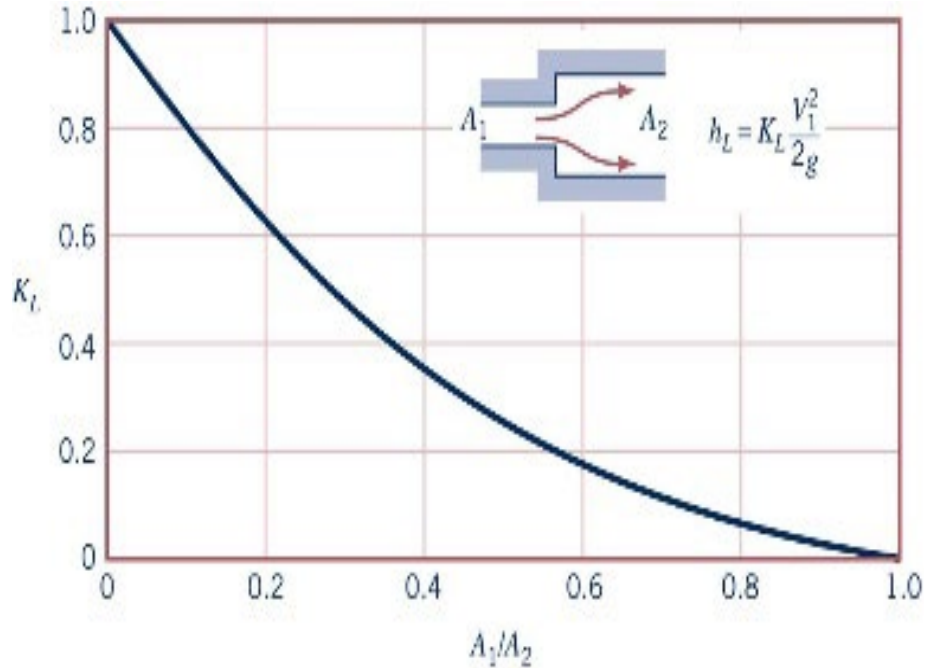
$$K_{L_{exit}} = 1.0$$

**For multi-component systems**

$$h_{L,multiple} \Big|_{\min \text{ or }} = h_{L1} + h_{L2} + h_{L3} + \dots$$

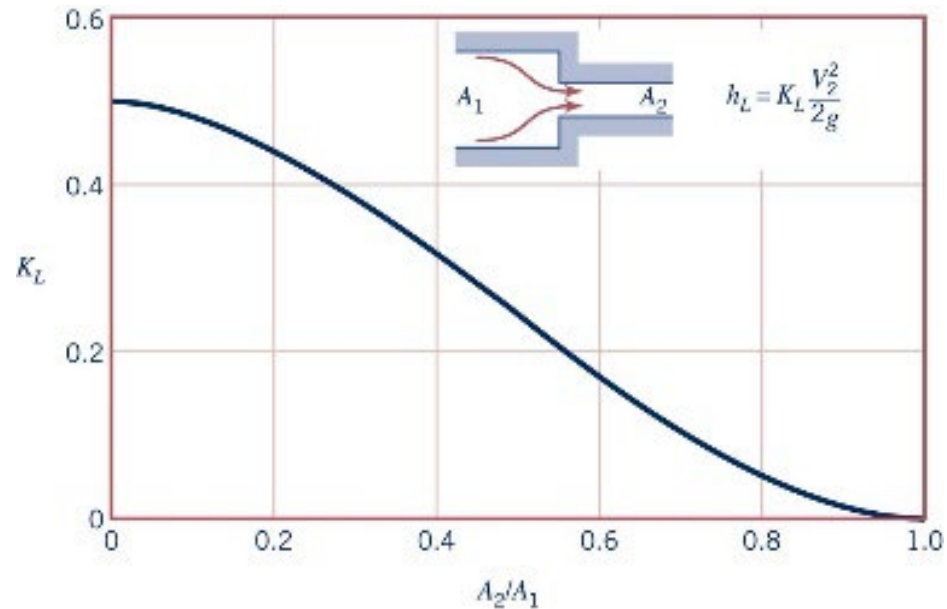
\*See Fig. 8.32 for typical valve geometry.

# Sudden Contraction/Expansion Loss



*NOTE*

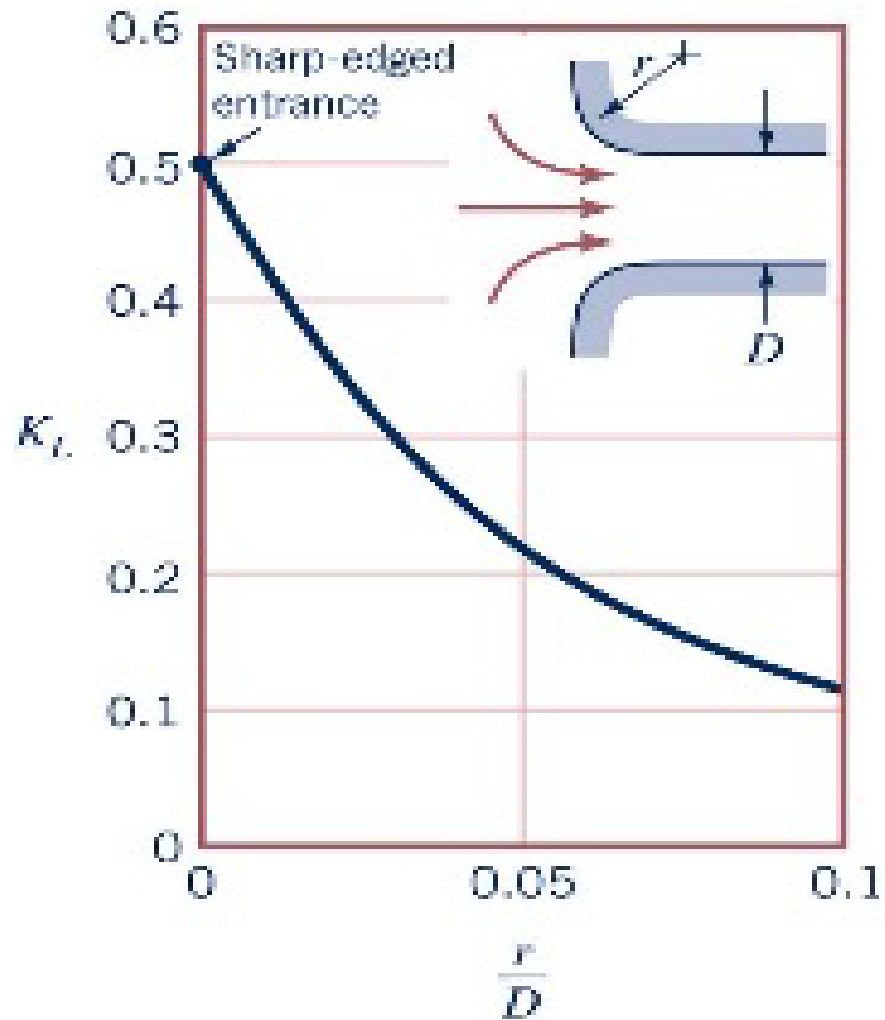
Let:  $\frac{A_1}{A_2} \rightarrow 0$ , i.e. Exit Loss,  $K_L = 1.0$



*NOTE*

Let:  $\frac{A_2}{A_1} \rightarrow 0$ , i.e. Inlet Loss,  $K_L = 0.5$

# Loss Coefficient vs Radius





# Total Head Loss in Pipe Flows

$\Delta P = \gamma h_L \rightarrow$  Pressure Drop Due to Friction

$\dot{W}_p = \gamma h_L Q = \Delta P Q \rightarrow$  Minimum Pumping Power Required

$$h_{L|total} = h_{L_{major}} + h_{L_{minor}} \rightarrow \text{UNITS = LENGTH}$$

$$\Rightarrow h_{L|total} = \sum_{j=1}^m f_j \frac{L_j}{D_j} \frac{V_j^2}{2g} + \sum_{i=1}^n \left( k_{L_{minor}} \right)_i \left( \frac{V_i^2}{2g} \right)$$

**Major losses due to friction in straight pipe sections**

**Minor losses due to bending, joints, etc. “connecting” straight pipe sections**



# Energy Equation

$$h_1 + h_{p_{IDEAL}} = h_{T_{IDEAL}} + h_2 + h_q + \sum_{j=1}^m \left( \frac{fL}{D} \frac{V^2}{2g} \right)_j + \sum_{i=1}^n \left( \frac{k_{L_{minor}} V^2}{2g} \right)_i$$

$$h_q = \frac{u_2 - u_1}{g} - \frac{\dot{Q}}{\dot{m}g} \rightarrow \text{Flow w/Heat Transfer}$$

$$h_{1,2} = \frac{P}{\gamma} + \frac{V^2}{2g} + z; \text{ or}$$

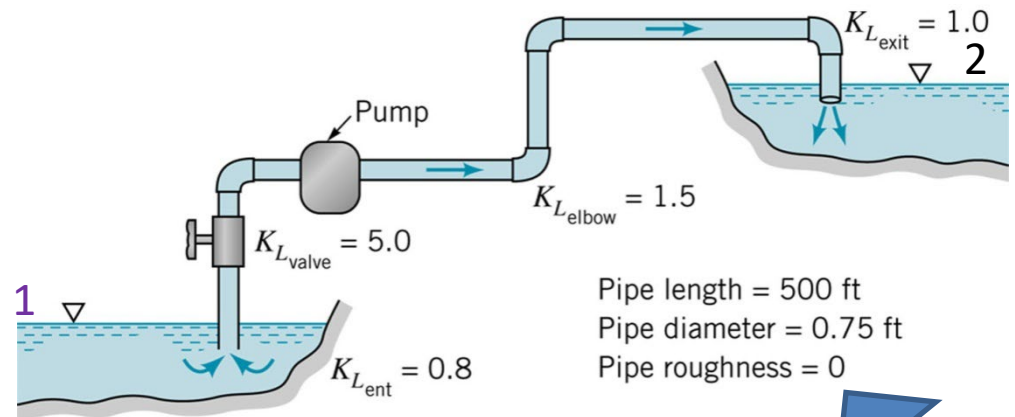
$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 + \frac{h_{p_{IDEAL}}}{\eta_p} = h_q + \eta_T h_{T_{IDEAL}} + \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + \sum_{j=1}^m \left( \frac{fL}{D} \frac{V^2}{2g} \right)_j + \sum_{i=1}^n \left( \frac{k_L V^2}{2g} \right)_i; \text{ where}$$

$h_p$  = isentropic (ideal) pump **INPUT** head

$h_T$  = isentropic (ideal) turbine **OUTPUT** head

# Calculation of head losses

**Example – Problem # 8.97:** The pump shown in Figure below delivers a head of 250ft to the water. Determine the power that the pump adds to the water. The difference in elevation of the two ponds is 200ft.



**Solution:** The viscous pipe flow equation with losses can be written as

$$\frac{p_1}{\gamma} + z_1 + \frac{V_1^2}{2g} + h_p = \frac{p_2}{\gamma} + z_2 + \frac{V_2^2}{2g} + h_L \quad (1)$$

where  $p_1 = p_2 = 0$ ;  $V_1 = V_2 = 0$ ;  $z_1 = 0$ ;  $z_2 = 200 \text{ ft}$ ;  $h_p = 250 \text{ ft}$ .

# Calculation of head losses

CONSTANT PIPE DIAMETER

Thus (1) reduces to:

$$-h_L + h_p = z_2$$

$$\Rightarrow - \left( f_{guess} \frac{L}{D} \frac{V^2}{2g} + \sum_{i=1}^n (k_{Lminor})_i \left( \frac{V^2}{2g} \right) \right) + h_p = z_2 \quad (2)$$

**Now** 
$$\sum_{i=1}^n (k_{Lminor})_i \left( \frac{V^2}{2g} \right) = (0.8 + 5.0 + 4 \times (1.5) + 1.0) \left( \frac{V^2}{2g} \right) = 12.8 \left( \frac{V^2}{2g} \right)$$

**Therefo** 
$$- \left( \left[ f_{GUESS} \frac{(500 \text{ ft})}{(0.75 \text{ ft})} + 12.8 \right] \frac{V^2}{2(32.2 \text{ ft/s}^2)} \right) + 250 \text{ ft} = 200 \text{ ft}$$

$$\Rightarrow (667 f_{GUESS} + 12.8) V^2 = 3220 \quad (3):$$

Friction Characteristic Equation  $\rightarrow$

$$V(f_{GUESS}) = \left( \frac{3220}{667 f_{GUESS} + 12.8} \right)^{1/2} \rightarrow \text{Guess } f: 0.01 \leq f_{GUESS} \leq 0.03$$

# Calculation of head losses

**Now**  $V = \left( \frac{3220}{667 f_{GUESS} + 12.8} \right)^{1/2} \quad (3)$

$$Re_D = \frac{\rho V D}{\mu} = \frac{(1.94 \text{ slug} / \text{ft}^3) V (0.75 \text{ ft})}{(2.34 \times 10^{-5} \text{ lb} \cdot \text{s} / \text{ft}^2)} = 6.22 \times 10^4 \bullet V \quad (4)$$

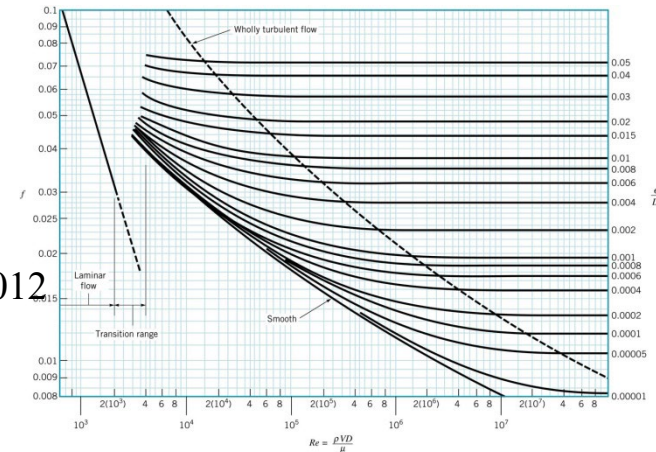
**Use Moody's diagram -**

**Trial & error method:**

Assume  $f_1 = 0.02 \rightarrow V = 11.1 \text{ ft/s} \rightarrow Re_D = 6.9 \times 10^5 \rightarrow f_{moody} = 0.012 \neq 0.02$

Assume  $f_2 = 0.012 \rightarrow V = 12.4 \text{ ft/s} \rightarrow Re_D = 7.7 \times 10^5 \rightarrow f_{moody} = 0.0121 \simeq 0.012$

Thus  $V = 12.4 \text{ ft/s}$



**Hence the power added to the water is**

$$\dot{W}_S = Q(\gamma h_p) = (VA)(\gamma h_p) = (12.4 \text{ ft/s}) \left( \pi/4 [0.75 \text{ ft}]^2 \right) (62.4 \text{ lb} / \text{ft}^3) (250 \text{ ft}) = 8.55 \times 10^4 \frac{\text{ft} \cdot \text{lb}}{\text{s}}$$

$$\Rightarrow \dot{W}_S = 8.55 \times 10^4 \frac{\text{ft} \cdot \text{lb}}{\text{s}} \times \frac{1 \text{ hp}}{(550 \text{ ft} \cdot \text{lb} / \text{s})} = 155 \text{ hp}$$

**You may also use HAALAND formula to find  $f$ .**

# HALLAND EQUATION

## Good for Programming Calculator

$$V = \left( \frac{3220}{667 f_{guess} + 12.8} \right)^{1/2} \quad (3)$$

$$Re_D = \frac{\rho V D}{\mu} = \frac{(1.94 \text{ slug/ft}^3) V (0.75 \text{ ft})}{(2.34 \times 10^{-5} \text{ lb} \cdot \text{s/ft}^2)} = 6.22 \times 10^4 V \quad (4)$$

$$\frac{1}{\sqrt{f}} = -1.8 \log_{10} \left( \left( \frac{\varepsilon / D}{3.7} \right)^{1.11} + \frac{6.9}{Re} \right)$$

HALLAND EQUATION

HAALLAND EQUATION

HAALLAND EQUATION														
e/D	DENS	Visc	D	f (guess)	e/D	DENS	Visc	D	f (guess)	e/D	DENS	Visc	D	f (guess)
0	1.94	2.34E-05	0.75	0	0	1.94	2.34E-05	0.75	0.01	0	1.94	2.34E-05	0.75	1
f	V	Re	f (FALLAND)	f	V	Re	f (FALLAND)	f	V	Re	f (FALLAND)			
0	15.86	9.862E+05	0.0116	0.01	12.86	7.996E+05	0.0120	1	2.18	1.353E+05	0.0168			
0.0116	12.52	7.784E+05	0.0121	0.0120	12.43	7.731E+05	0.0121	0.0168	11.59	7.206E+05	0.0123			
0.0121	12.42	7.724E+05	0.0121	0.0121	12.42	7.723E+05	0.0121	0.0123	12.39	7.705E+05	0.0121			
0.0121	12.42	7.722E+05	0.0121	0.0121	12.42	7.722E+05	0.0121	0.0121	12.42	7.722E+05	0.0121			
0.0121	12.42	7.722E+05	0.0121	0.0121	12.42	7.722E+05	0.0121	0.0121	12.42	7.722E+05	0.0121			



# Calculation of head losses/pressure drop

- EXAMPLE: Water at 0.02 m<sup>3</sup>/s flows through 350m of horizontal cast iron pipe (D=20.27 cm). Determine the head loss and pressure drop?

$$\nu = \frac{\mu}{\rho} = 9.569 \times 10^{-7} \frac{\text{m}^2}{\text{s}}$$

$$V = \frac{Q}{A} = \frac{0.02 \frac{\text{m}^3}{\text{s}}}{0.032270 \text{m}^2} = 0.62 \frac{\text{m}}{\text{s}} \rightarrow \text{Re} = \frac{VD}{\nu} = 1.31 \times 10^5 \rightarrow \text{TURBULENT}$$

Table 8.1

$\varepsilon$  = Relative Roughness = 0.026 cm

$$\frac{\varepsilon}{D} = \frac{0.026 \text{cm}}{20.27 \text{cm}} = 0.0012$$

Moody Diagram ( $\text{Re}, \frac{\varepsilon}{D}$ ),  $f = 0.022$ ; (or Haaland Equation)

HEAD LOSS

$$h_L = \frac{fL}{D} \frac{V^2}{2g} = \frac{0.022 \times 350}{0.2027} \frac{(0.62)^2}{2(9.81)} = 0.744 \text{ m of water}$$

PRESSURE DROP

$$\Delta P = \gamma h_L = 9800 \frac{\text{N}}{\text{m}^3} \cdot 0.744 \text{m} = 7,280 \frac{\text{N}}{\text{m}^2}$$

# Problem Types

## TYPES

1. Given:  $L, \nu, \varepsilon, Q, D \rightarrow$  FIND  $h_L = f\left(V, \frac{\varepsilon}{D}\right) \frac{L}{D} \frac{V^2}{2g}$

2. Given:  $L, \nu, \varepsilon, D, h_L(Q, D) \rightarrow$  FIND  $Q \rightarrow$  TRIAL-n-ERROR

3. GIVEN:  $L, \nu, \varepsilon, Q, h_L(Q, D) \rightarrow$  FIND  $D \rightarrow$  TRIAL-n-ERROR

$$\nu = \frac{\mu(\text{Dynamic Viscosity})}{\rho(\text{Density})} \rightarrow \text{Kinematic Viscosity}$$

# Calculation of head losses/pressure drop

- EXAMPLE: A flowrate of 3.5 ft<sup>3</sup>/s is to be maintained in a horizontal aluminum pipe with an inlet pressure of 65 psig, and an outlet pressure of 30 psig. The pipe length is 500ft. Determine the pipe diameter.

$$h_1 + \cancel{h_{f,IDEAL}} = \cancel{h_{f,IDEAL}} + h_2 + \cancel{h_q} + \sum_{j=1}^m \left( \frac{f_j L_j}{D_j} \frac{V_j^2}{2g} \right) + \sum_{i=1}^n \left( \frac{k_{minor} V^2}{2g} \right)$$

$$V = \frac{Q}{A} = \frac{3.5}{\pi \frac{D^2}{4}} = \frac{4.46}{D^2}$$

$$\frac{p_1 - p_2}{\gamma} = \frac{fL}{D} \frac{V^2}{2g} = \frac{fL}{D} \frac{\left(\frac{4.46}{D^2}\right)^2}{2g}$$

$$\frac{(65 - 30) \text{ psig} \cdot 144 \frac{\text{in}^2}{\text{ft}^2}}{62.4 \frac{\text{lb}_f}{\text{ft}^3}} = \frac{f \cdot 500}{D} \frac{\left(\frac{4.46}{D^2}\right)^2}{2 \cdot 32.2}$$

solving for D(f)=

$$D = 1.138 f^{1/5}$$

TRIAL-n-ERROR  $\rightarrow f(V, D, \frac{\varepsilon}{D})$

## SOLUTION METHOD

$$\varepsilon = 5 \times 10^{-6} \text{ ft}$$

1. Guess  $f_1 = 0.02$ ,  $D_1 = 0.520 \text{ ft}$ ,  $Re = \frac{VD}{\nu} = 7.11 \times 10^5$ ,  $\frac{\varepsilon}{D} = 9.6 \times 10^{-4}$
2. Check GUESS  $\rightarrow f_{1,MOODY} = 0.0128 \neq 0.02 \rightarrow$  MUST ITERATE AGAIN
3. Guess  $f_2 = 0.0128$ ,  $D_2 = 0.476 \text{ ft}$ ,  $Re_2 = \frac{VD}{\nu} = 7.77 \times 10^5$ ,  $\frac{\varepsilon}{D_2} = 1.1 \times 10^{-5}$
4. Check GUESS  $\rightarrow f_{2,MOODY} = 0.0128 = f_2 \rightarrow STOP$

ANSWER

$$D = 0.476 \text{ ft}$$

Water is pumped from the tank and exits as a free jet, and the pump manufacture has provided the pump head vs volume flow rate curve as shown.

Determine the flow rate through the 100 meter straight smooth pipe section.

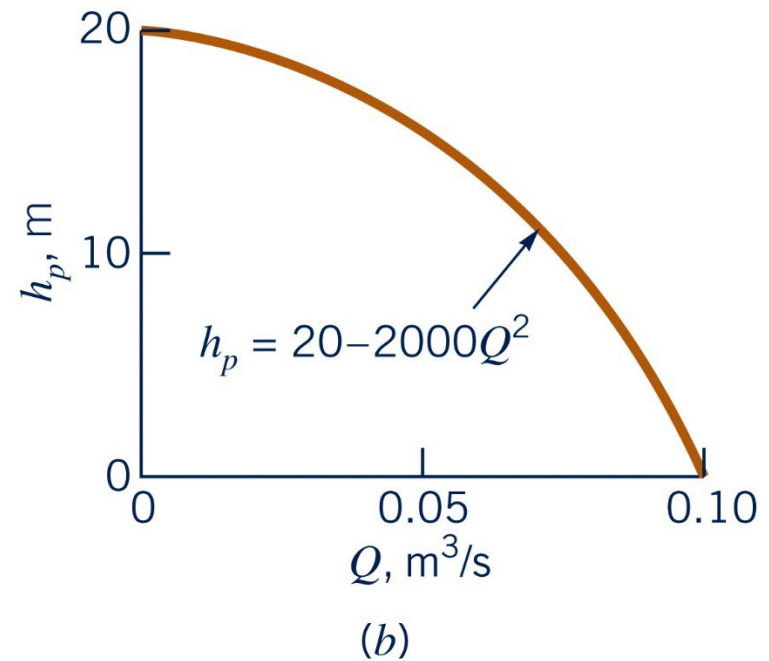
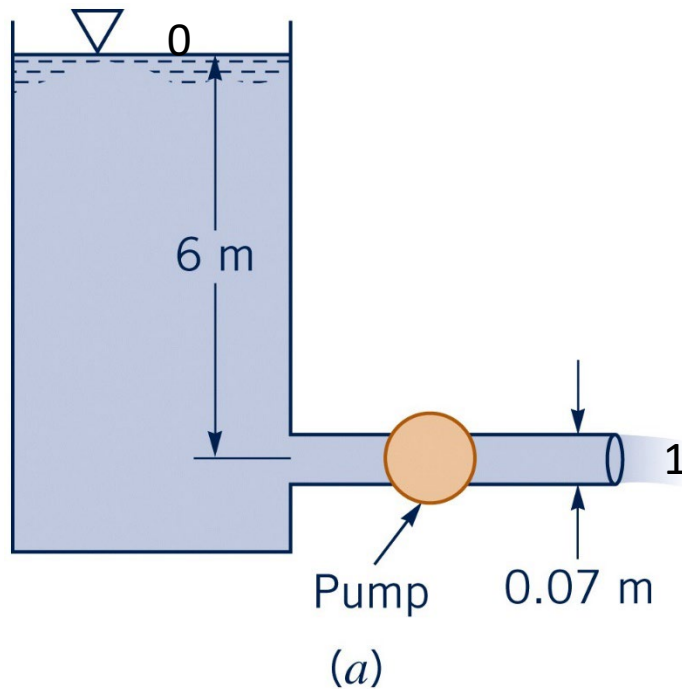


Figure P5.118a  
© John Wiley & Sons, Inc. All rights reserved.

Figure P5.118b  
© John Wiley & Sons, Inc. All rights reserved.

## ENERGY CONSERVATION (Single Inlet/Exit)

$$\frac{p_0}{\gamma} + z_0 + \frac{V_0^2}{2g} + h_p = \frac{p_1}{\gamma} + z_1 + \frac{V_1^2}{2g} + h_{L_{MINOR}} + h_{L_{MAJOR}} \quad (1)$$

$$p_0 = p_1 = V_0 = z_1 = h_T = 0$$

$$z_0 = 6m$$

$$6 + h_p = \frac{V_1^2}{2g} + h_{L_{MINOR}} + h_{L_{MAJOR}}$$

## MASS CONSERVATION

$$V_1 = \frac{Q}{A_1} \quad (2)$$

## Combine MASS with Energy & Pump Head

$$6 + h_p = \frac{\left[ \frac{Q}{A_1} \right]^2}{2g} + h_{L_{MINOR}} + h_{L_{MAJOR}}$$

$$6 + (20 - 2000Q^2) = \frac{\left[ \frac{Q}{A_1} \right]^2}{2g} + h_{L_{MINOR}} + h_{L_{MAJOR}} \quad (3)$$

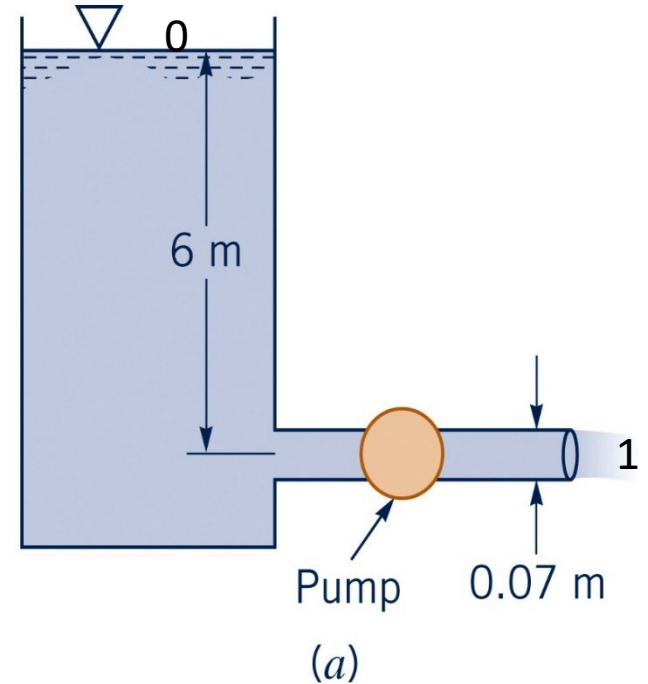


Figure P5.118a  
© John Wiley & Sons, Inc. All rights reserved.

## PUMP HEAD UNITS

$$\begin{aligned}hp[m] &= 20 - 2000Q^2 \\ &= 20[m] - 2000[ ]Q^2 \left[ \frac{m^3}{s} \right]^2\end{aligned}$$

## UNIT ANALYSIS

$$m = 20[m] - 2000[ ]Q^2 \frac{m^6}{s^2}$$

$$m \frac{s^2}{m^6} = [ ]$$

$$\frac{s^2}{m^5} = [ ]$$

$$hp[m] = 20[m] - 2000 \left[ \frac{s^2}{m^5} \right] Q^2 \left[ \frac{m^3}{s} \right]^2$$



$$6 + (20 - 2000Q^2) = \frac{\left[\frac{Q}{A_1}\right]^2}{2g} + h_{L_{MINOR}} + h_{L_{MAJOR}} \quad (3)$$

MINOR and MAJOR LOSSES

$$h_{L_{MINOR}} = (k_{inlet} + k_{exit}) \frac{V^2}{2g} = (0.5 + 1.0) \frac{\left[\frac{Q}{A_1}\right]^2}{2g}$$

$$h_{L_{MAJOR}} = f \frac{L V^2}{D 2g} = f \frac{L}{D} \frac{\left[\frac{Q}{A_1}\right]^2}{2g}$$

COMBINE WITH ENERGY EQUATION

$$6 + (20 - 2000Q^2) = \frac{\left[\frac{Q}{A_1}\right]^2}{2g} + (0.5 + 1.0) \frac{\left[\frac{Q}{A_1}\right]^2}{2g} + f \frac{L}{D} \frac{\left[\frac{Q}{A_1}\right]^2}{2g}$$

$$6 + (20 - 2000Q^2) = Q^2 \frac{(2.5 + f \frac{L}{D})}{A_1^2 2g}$$

$$26 = Q^2 \left( \frac{(2.5 + f \frac{L}{D})}{A_1^2 2g} + 2000 \right)$$

$$\sqrt{\frac{26[m]}{\left( \frac{(2.5 + f \frac{L}{D})}{A_1^2 2g [m^4 \frac{m}{s^2}]} + 2000 \left[ \frac{s^2}{m^5} \right] \right)}} = Q \rightarrow \text{FRICTION CHARACTERISTIC EQUATION}$$

$$\sqrt{\frac{m}{\frac{s^2}{m^5}}} = \sqrt{\frac{m^6}{s^2}} = \frac{m^3}{s} = Q$$



# Trial-n-Error Solution

$$\frac{26[m]}{\left( \frac{(1.5 + f \frac{L}{D})}{A_1^2 2g [m^4 \frac{m}{s^2}]} + 2000 \left[ \frac{s^2}{m^5} \right] \right)} = Q \rightarrow \text{FRICTION CHARACTERISTIC EQUATION}$$

1. guess " $f_{guess}^1$ "

2. Solve for Q

3. Solve for  $V=Q/A$

4. Solve for  $Re_D = \frac{\rho V D}{\mu}$

5. Check " $f_{guess}^1$ " guess with HAALAND eqn.

$$\frac{1}{\sqrt{f}} = -1.8 \log_{10} \left( \left( \frac{\epsilon/D}{3.7} \right)^{1.11} + \frac{6.9}{Re} \right)$$

$$f_{halland}^1 = \left[ \frac{1}{-1.8 \log_{10} \left( \left( \frac{\epsilon/D}{3.7} \right)^{1.11} + \frac{6.9}{Re} \right)} \right]^2$$

6. Compare  $f_{halland}$  to  $f_{guess}$

7. If not close(x.xxx), re-iterate

8. NEW  $f_{guess}^2 = f_{halland}^1 \rightarrow \text{GO TO 2}$

HAALLAND EQUATION				
	DENS	Visc	D	
e/D	kg/m3	Pa-s	m	<b>f (guess)</b>
0	999	1.12E-03	0.07	<b>0</b>
		L	A	
		m	m2	
	m3/s	100	0.00384845	m/s
f	Q	Re	f (FALLAND)	V
0	0.060252	9.775E+05	0.0116	15.65607
0.0116	0.020102	3.261E+05	0.0141	5.223338
0.0141	0.018423	2.989E+05	0.0144	4.787201
0.0144	0.018288	2.967E+05	0.0144	4.752007
0.0144	0.018276	2.965E+05	0.0144	4.749025

HAALLAND EQUATION				
	DENS	Visc	D	
e/D	kg/m3	Pa-s	m	<b>f (guess)</b>
0	999	1.12E-03	0.07	<b>1</b>
		L	A	
		m	m2	
	m3/s	100	0.003848451	m/s
f	Q	Re	f (FALLAND)	V
1	0.002298	3.728E+04	0.0222	0.59713
0.0222	0.014967	2.428E+05	0.0149	3.889074
0.0149	0.017964	2.914E+05	0.0144	4.667822
0.0144	0.018249	2.961E+05	0.0144	4.741799
0.0144	0.018273	2.965E+05	0.0144	4.748156

HAALLAND EQUATION				
	DENS	Visc	D	
e/D	kg/m3	Pa-s	m	<b>f (guess)</b>
0	999	1.12E-03	0.07	<b>0</b>
		<b>L</b>	<b>A</b>	
		m	m2	
	m3/s	100	0.00384845	m/s
<b>f</b>	<b>Q</b>	<b>Re</b>	<b>f (FALLAND)</b>	<b>V</b>
0	0.060252	9.775E+05	0.0116	15.65607
0.0116	0.020102	3.261E+05	0.0141	5.223338
0.0141	0.018423	2.989E+05	0.0144	4.787201
0.0144	0.018288	2.967E+05	0.0144	4.752007
0.0144	0.018276	2.965E+05	0.0144	4.749025

HAALLAND EQUATION				
	DENS	Visc	D	
e/D	kg/m3	Pa-s	m	<b>f (guess)</b>
0	999	1.12E-03	0.07	<b>1</b>
		<b>L</b>	<b>A</b>	
		m	m2	
	m3/s	100	0.003848451	m/s
<b>f</b>	<b>Q</b>	<b>Re</b>	<b>f (FALLAND)</b>	<b>V</b>
1	0.002298	3.728E+04	0.0222	0.59713
0.0222	0.014967	2.428E+05	0.0149	3.889074
0.0149	0.017964	2.914E+05	0.0144	4.667822
0.0144	0.018249	2.961E+05	0.0144	4.741799
0.0144	0.018273	2.965E+05	0.0144	4.748156

# Calculation of head losses/pressure drop

- EXAMPLE: Water to be moved from a large tank in which the air pressure is 20 psig into a large open tank through 2000 ft. of smooth pipe at the rate of 3 ft<sup>3</sup>/s. The open fluid level is 150 ft. below the level in the closed tank. Determine the pipe diameter.

ASSUME TURBULENT FLOW

Neglect "MINOR" losses due to length of pipe

$$h_1 + \cancel{h_{f,IDEAL}} = \cancel{h_{f,IDEAL}} + h_2 + \cancel{h_g} + \sum_{j=1}^m \left( \frac{f_j L_j}{D} \frac{V_j^2}{2g} \right) + \sum_{i=1}^n \left( \frac{k_i L_{minor} V^2}{2g} \right)$$

$$\frac{p_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{p_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + \frac{fL}{D} \frac{V^2}{2g}$$

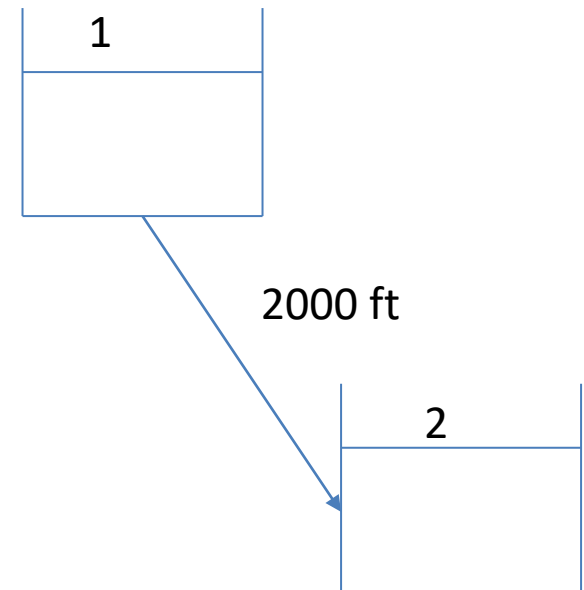
$$V_1 = V_2 = p_2 = 0; z_1 - z_2 = 150 \text{ ft}; p_1 = 20 \text{ psi} \cdot \frac{144 \text{ in}^2}{\text{ft}^2}; V = Q/A = \frac{3 \text{ ft}^3/\text{s}}{\frac{\pi D^2}{4}} = \frac{3.82}{D^2}$$

Combine

$$\frac{20 \text{ psi} \cdot \frac{144 \text{ in}^2}{\text{ft}^2}}{\gamma = 62.4 \text{ lb/ft}^3} + 150 \text{ ft} = \frac{fL}{D} \frac{1}{2g} \left( \frac{3.82}{D^2} \right)^2$$

or

$$D = 1.18 f^{1/5} \text{ AND } \text{Re} = \frac{VD}{\nu} = \frac{\frac{3.82}{D^2} \cdot D}{\frac{2.34 \times 10^{-5}}{1.94}} = \frac{3.17 \times 10^5}{D}$$



# TRIAL-n-ERROR

## HALLAND

fguess					
0.02					
f	D	Re	HAALLAND		
0.02000000	0.53962	587,450	0.012698126		
0.01269813	0.492754	643,323	0.012497282		
0.01249728	0.491185	645,378	0.01249032		
0.01249032	0.49113	645,450	0.012490077		
0.01249008	0.491128	645,452	0.012490068		
fguess					
0.1					
f	D	Re	HAALLAND	Velocity	hl
0.10000000	0.74453	425,772	0.013450067	6.891271	198.0892
0.01345007	0.498456	635,964	0.012522452	15.3748	198.0892
0.01252245	0.491383	645,118	0.012491198	15.82062	198.0892
0.01249120	0.491137	645,441	0.012490108	15.83645	198.0892
0.01249011	0.491129	645,452	0.01249007	15.837	198.0892

$$\frac{1}{\sqrt{f}} = -1.8 \log_{10} \left( \left( \frac{\varepsilon / D}{3.7} \right)^{1.11} + \frac{6.9}{\text{Re}} \right); \text{smooth}, \varepsilon = 0$$

$$\frac{1}{\sqrt{f}} = -1.8 \log_{10} \left( \frac{6.9}{\text{Re}} \right)$$

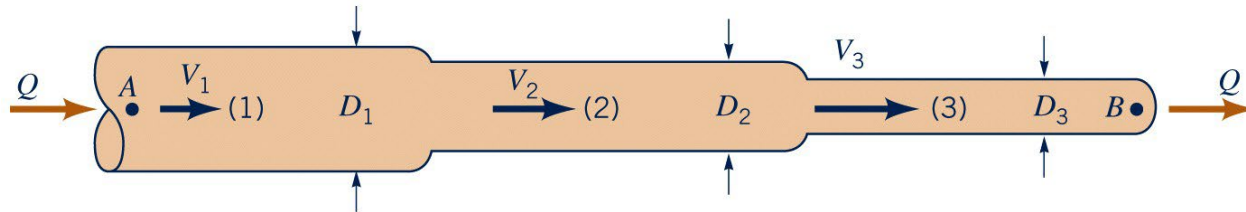
$$D = 1.18 f^{1/5}$$

$$V = Q / A = \frac{3 \text{ ft} / \text{s}}{\pi D^2 / 4} = \frac{3.82}{D^2}$$

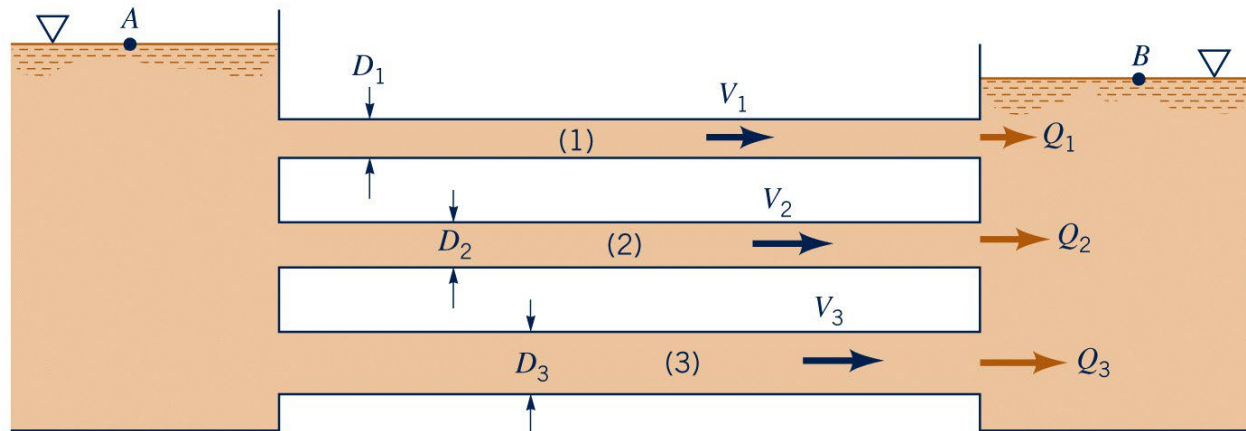
Power Loss Due to Friction = Minimum Pump Power

$$\begin{aligned} \dot{W}_{\text{loss}} &= \gamma Q h_f \\ &= 62.4 \frac{\text{lb}_f}{\text{ft}^3} \cdot 3 \frac{\text{ft}^3}{\text{s}} \cdot 198.09 \text{ ft} \\ &= 3.7 \times 10^4 \frac{\text{lb}_f \cdot \text{ft}}{\text{s}} \cdot \frac{1 \text{ HP}}{550 \frac{\text{lb}_f \cdot \text{ft}}{\text{s}}} \\ &= 67.4 \text{ HP} \end{aligned}$$

# Multiple Pipe Systems Series vs Parallel



(a)



(b)

Figure 8.35  
© John Wiley & Sons, Inc. All rights reserved.

# Multiple Pipe Systems

## Series vs Parallel

### *SERIES*

$$Q_1 = Q_2 = Q_3$$

$$h_{total} = h_1 + h_2 + h_3 = \sum f_i \frac{L_i}{D_i} \frac{V_i^2}{2g} + \sum K_{L_i} \frac{V_i^2}{2g}$$

### *PARALLEL*

$$Q_{total} = Q_1 + Q_2 + Q_3$$

$$h_1 = h_2 = h_3$$

$$f_1 \frac{L_1}{D_1} \frac{V_1^2}{2g} = f_2 \frac{L_2}{D_2} \frac{V_2^2}{2g} = f_3 \frac{L_3}{D_3} \frac{V_3^2}{2g}$$