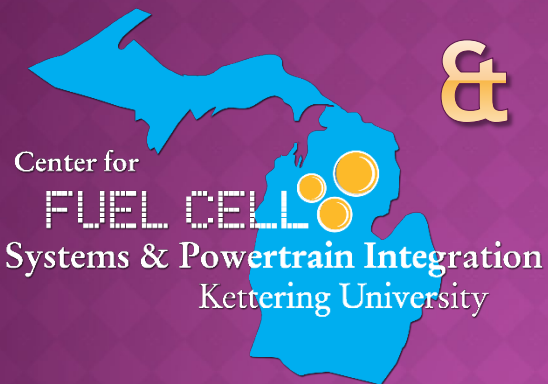


PEM HUMIDIFICATION

MECH-526



FUEL CELL SCIENCE & ENGINEERING



Center for
FUEL CELL
Systems & Powertrain Integration
Kettering University

Dr. K. J. Berry, P.E.

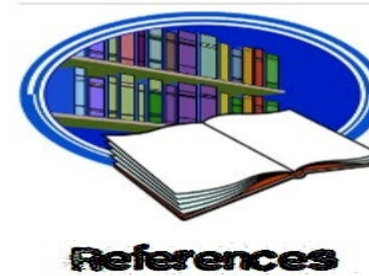
Mechanical Engineering

Kettering University

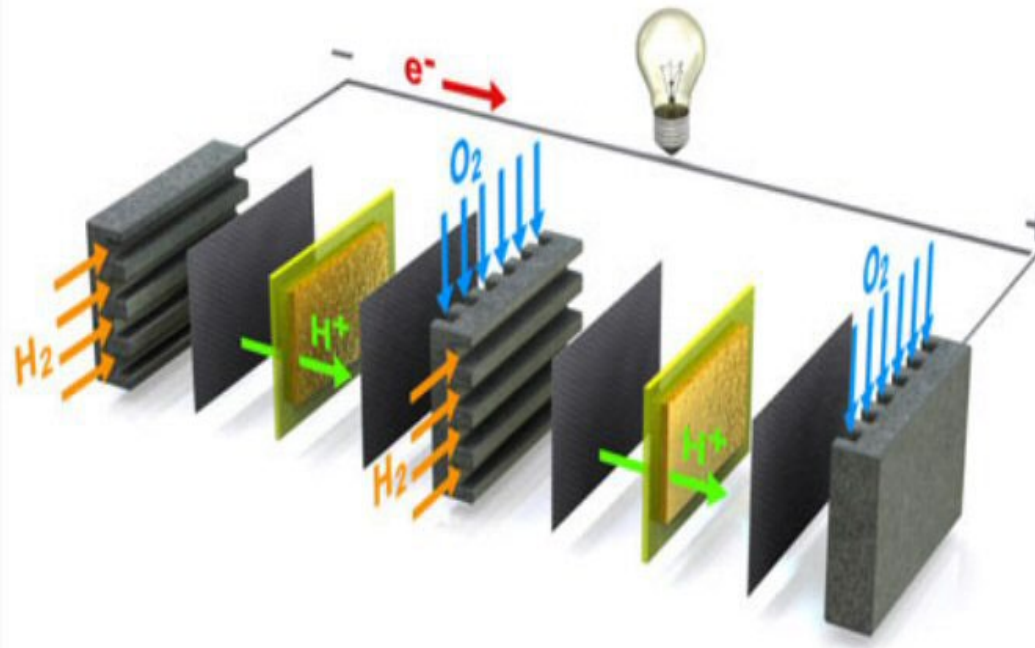
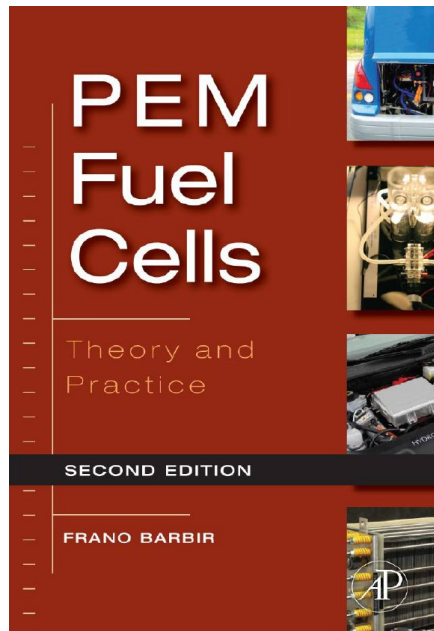
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REFERENCES:



- ◉ PEM Fuel Cells: Frano Barbir, ELSEVIER.
- ◉ Fuel Cell Explained: Larmie & Dicks, WILEY.
- ◉ Fuel Cell Fundamentals: O'hayre, Cha, et al., WILEY.



WATER VAPOR CONTENT IN GAS @ SATURATION

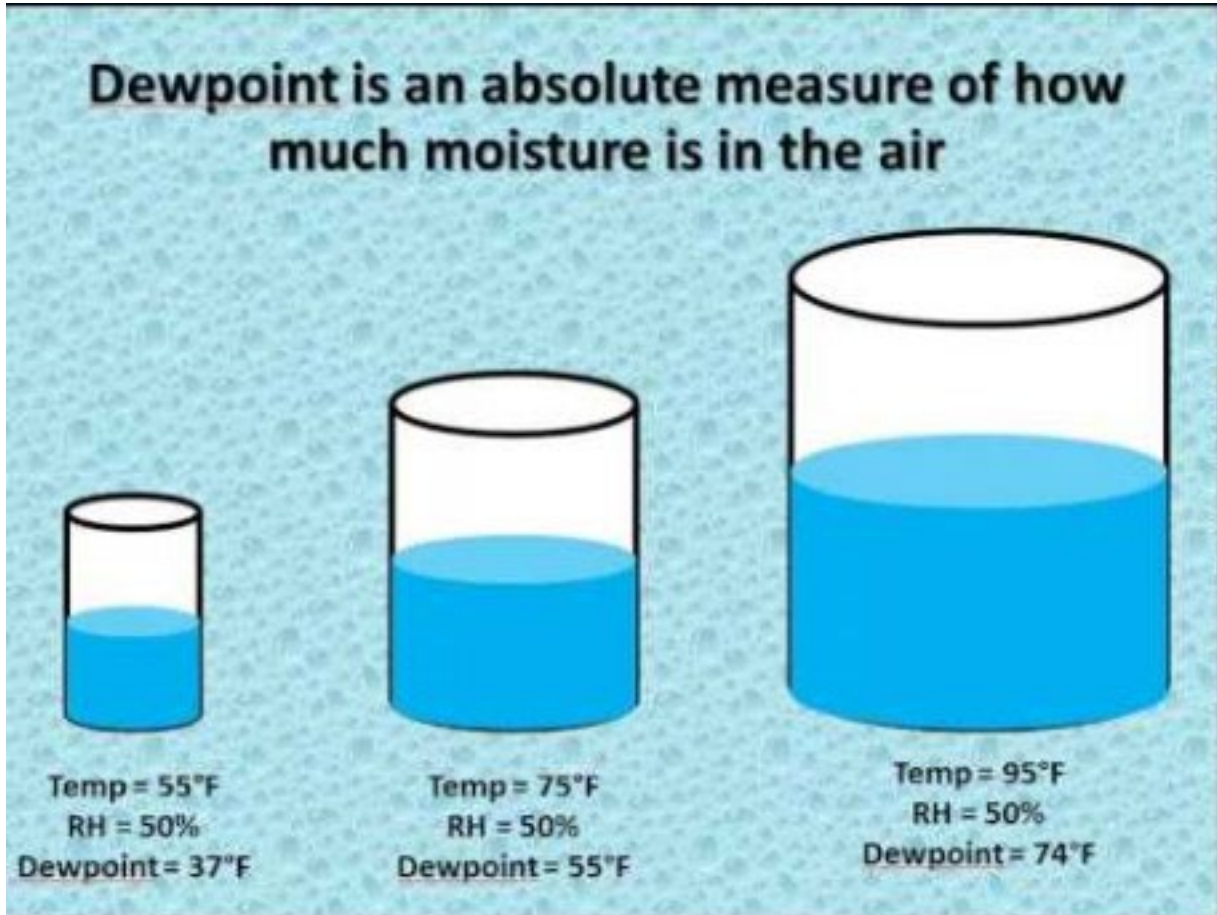
**PEM FUEL CELL
HUMIDIFICATION
IS CRITICAL**

Water in air will evaporate
w/temperature to ensure that enough
WATER VAPOR is present in the **AIR** to
ensure equilibrium.



HUMIDITY VS DEWPOINT

[HTTPS://WWW.YOUTUBE.COM/WATCH?V=OIEJHVHRDOO](https://www.youtube.com/watch?v=OIEJHVHRDOO)



HUMIDITY is how much water is dissolved into air. Has UPPER limit as a function on TEMPERATURE.

RELATIVE HUMIDITY is ratio of how much water is dissolved compared to the MAXIMUM possible. Expressed as % of maximum at this temperature.

DEWPOINT is an ABSOLUTE measure of how much moisture is in the air and is the temperature air needs to be **COOLED** to reach 100% **RELATIVE HUMIDITY**.

THERMODYNAMICS OF MOIST AIR

◉ Humidity Ratio (MASS/MOLAR)

Humidity Ratio - MOLAR

$$X = \frac{\text{Moles of Vapor Water (M}_v\text{)}}{\text{Moles of Air (M}_{air}\text{)}} = \frac{M_v}{M_a} = \frac{\text{partial pressure water}}{\text{partial pressure air}} = \frac{p_v}{p_a} = \frac{p_v}{P_{total} - p_v}$$

Humidity Ratio - MASS

$$x = \frac{\text{mass of vapor water (g)}}{\text{mass of air (g)}} = \frac{G_v}{G_a} = \frac{\text{Moles of Vapor Water (M}_v\text{)} \cdot M_{H_2O}(\text{g / mole})}{\text{Moles of Air (M}_{air}\text{)} \cdot M_{air}(\text{g / mole})}$$

$$x = X \left[\frac{\text{Moles of Vapor Water}}{\text{Moles of Air}} \right] \cdot \frac{M_{H_2O}(\text{g / mole})}{M_{air}(\text{g / mole})} = \frac{\text{GRAMS of Vapor Water}}{\text{GRAMS of Air}}$$

$$= X \cdot \frac{18.0153}{28.9645}$$

$$= X \cdot 0.62198$$

$$= \frac{p_v}{P_{total} - p_v} \cdot 0.62198 \left[\frac{\text{GRAMS of Vapor Water}}{\text{GRAMS of Air}} \right]$$

RELATIVE HUMIDITY

- **Saturation Pressure** of a vapor which is in equilibrium with its liquid (as steam with water); specifically :the maximum pressure possible by water vapor at a given temperature.

$$\phi = \text{Relative Humidity (RH)} = \frac{\text{"ACTUAL" vapor water partial pressure}}{\text{vapor water SATURATION pressure}} = \frac{p_v}{p_{vs}(T)}$$

$$p_{vs}(T(K))_{\text{Pascals}} = e^C; (T = 273K \rightarrow 373K)$$

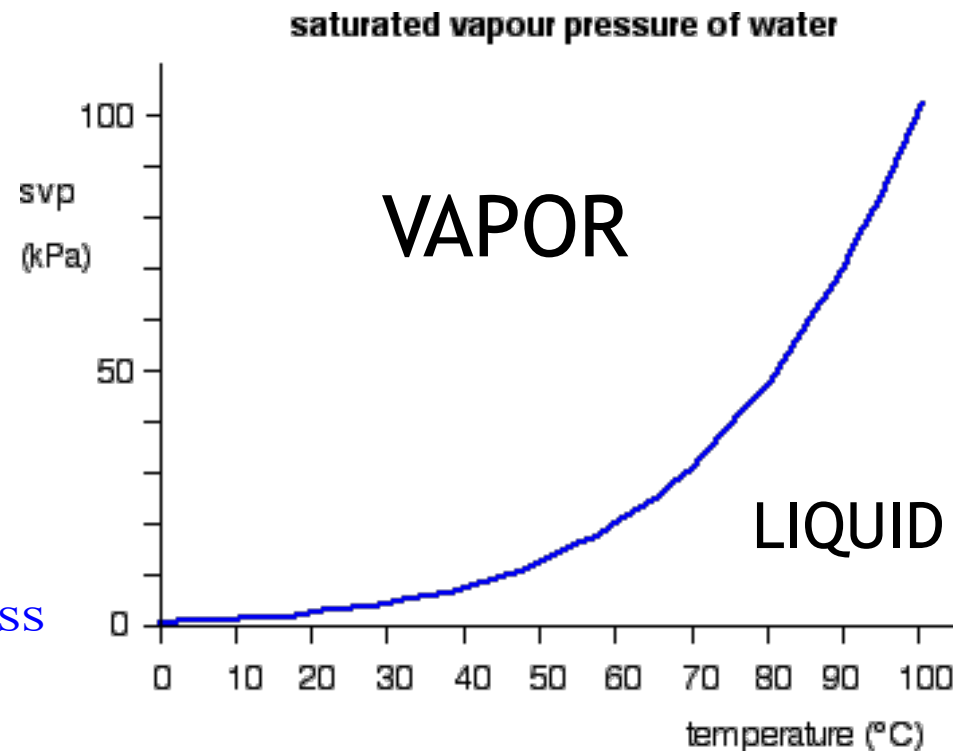
$$C = aT^{-1} + b + cT + dT^2 + eT^3 + f \ln(T)$$

<i>a</i>	-5800.2206
<i>b</i>	1.3914993
<i>c</i>	-0.04864239
<i>d</i>	0.4176468x10 ⁻⁴
<i>e</i>	-0.14452093x10 ⁻⁷
<i>f</i>	6.5459673

RATIOS :→ COMBINING(*X* and ϕ)

$$X = \frac{\phi p_{vs}(T)}{P_{total} - \phi p_{vs}(T)} \rightarrow \text{Humidity Ratio - MOLAR}$$

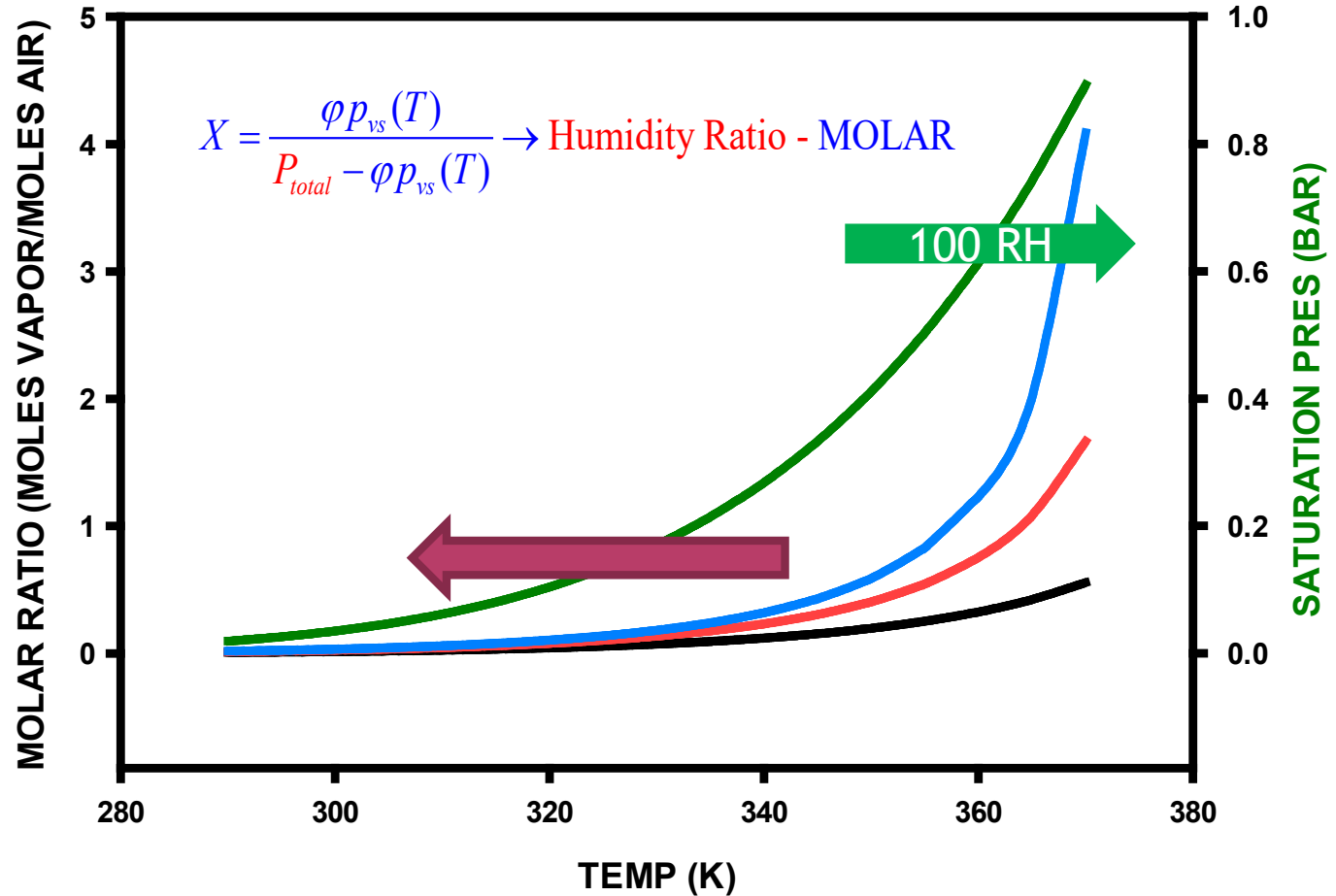
$$x = X \cdot \frac{M_{H_2O}(g / mole)}{M_{air}(g / mole)} \Rightarrow \text{Humidity Ratio - MASS}$$



Temperature vs Molar Ratio at Constant Pressure

P = 1 BAR

Increased Temperature w/RH = Increased Water Content (MOIST) at Const. Pressure



$$X = \frac{\phi p_{vs}(T)}{P_{total} - \phi p_{vs}(T)} \rightarrow \text{Humidity Ratio - MOLAR}$$

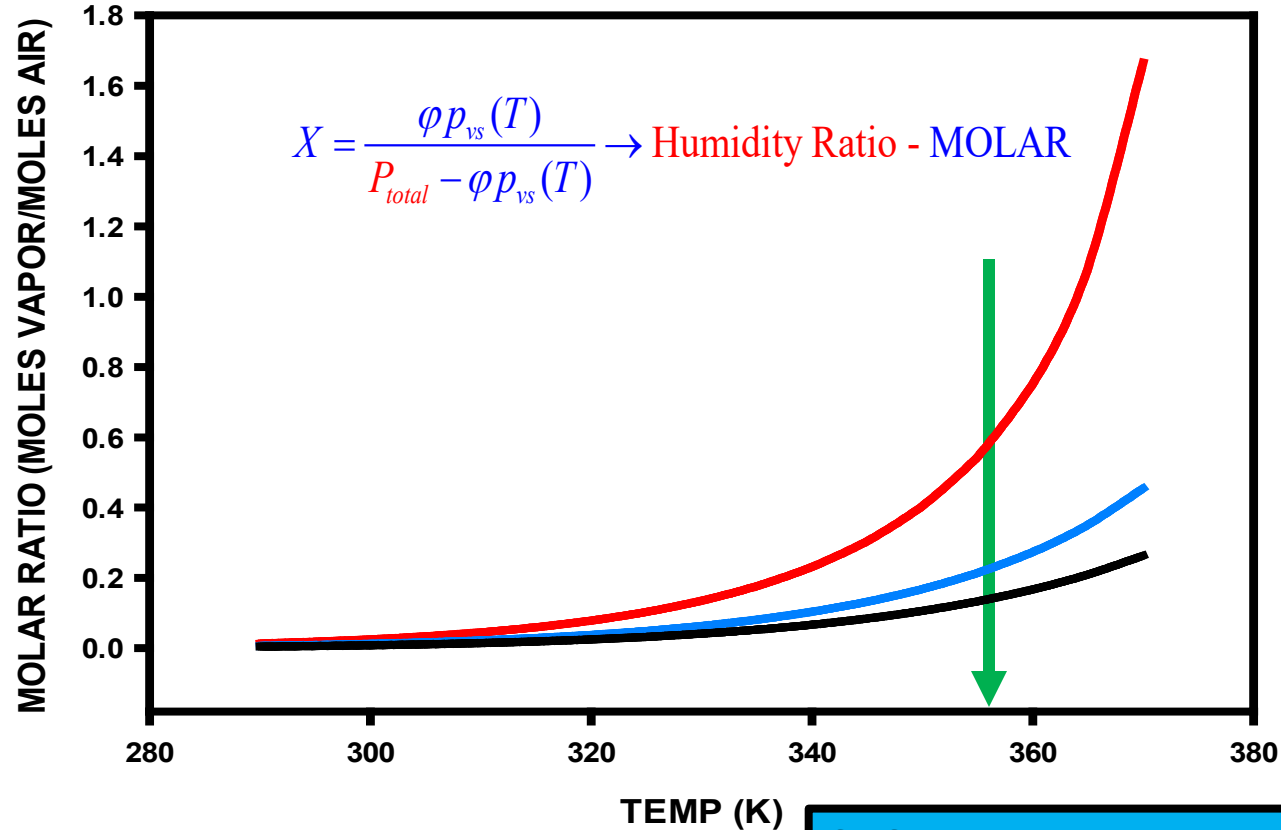
- TEMP (K) vs X (RH=0.4)
- TEMP (K) vs X (RH=0.7)
- TEMP (K) vs X (RH=0.9)
- TEMP (K) vs PSAT

RH = Relative Humidity

Temperature vs Molar Ratio at Constant RH

RH = 0.7

Increased Temperature w/Pressure = DECREASED Water Content (DRY) at Const. RH



- TEMP (K) vs X(Pres=1 Bar)
- TEMP (K) vs X(Pres=2 Bar)
- TEMP (K) vs X(Pres=3 Bar)

SYSTEM must inject MORE water to maintain RH as Pressure increases

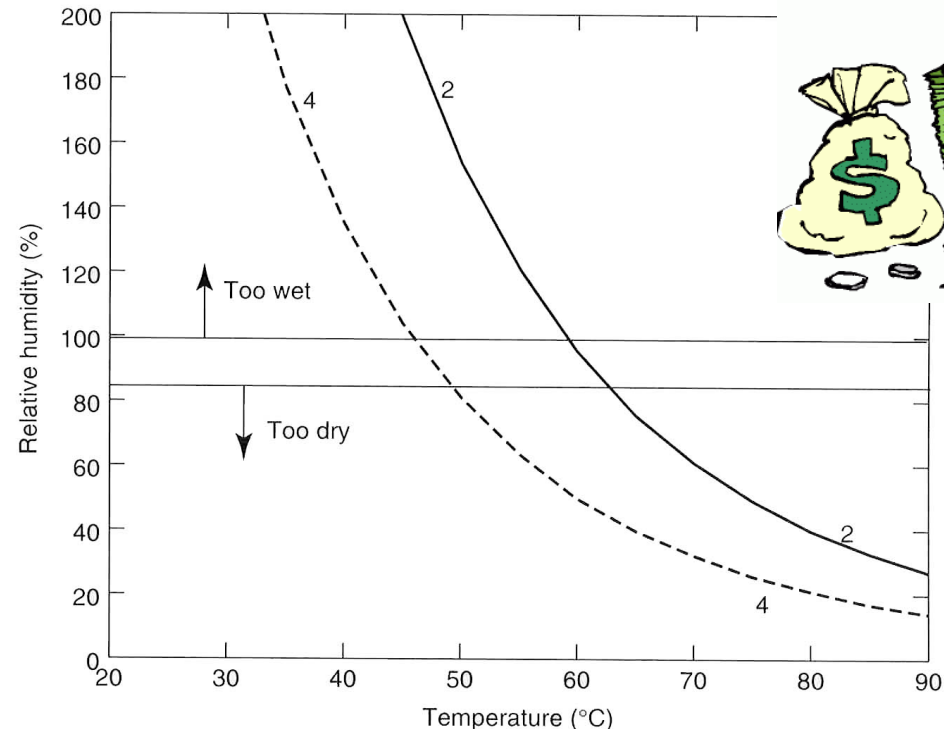
Increased Temperature → Increase Saturation Pressure → Drier @ Constant RH

CONDITIONS FOR PEMFC OPERATION WITHOUT EXTRA HUMIDIFICATION

- ◉ In limited operating conditions, a PEMFC can be run without extra humidification. Review the figure below for exit air humidity versus its temperature with $S = 2$ and 4 at operating pressure of 1 bar. Between the operating temperature of 50 and 60°C , the PEMFC can be run without humidification.

As PRESSURE increases, RELATIVE HUMIDITY decreases, i.e. air becomes dryer.

As TEMPERATURE increases, RELATIVE HUMIDITY increases, i.e. air becomes moist.



just
another
example

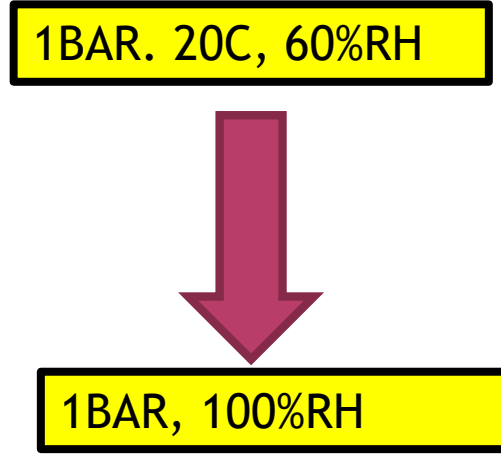
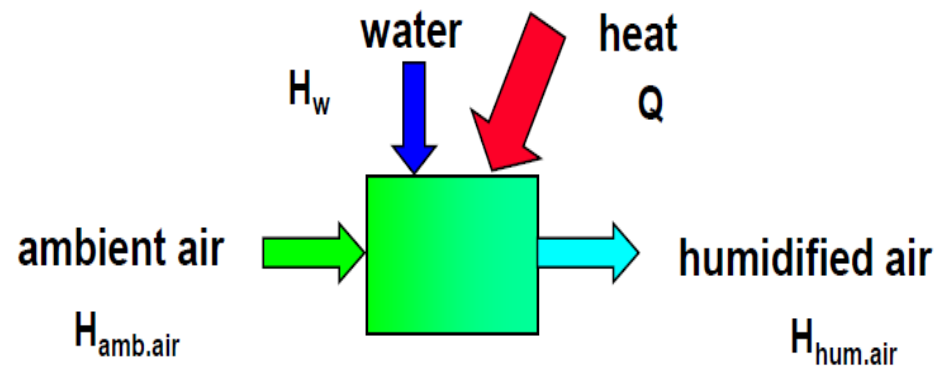
EXAMPLE 1

A100 plate fuel cell with 300-cm² active area operates at 0.6 A/cm² and 0.65 V.

Air is supplied at stoichiometric ratio of 2 and at a pressure of 1.15 bar, and it is **HUMIDIFIED BY INJECTING HOT WATER (60°C)** just before the stack inlet.

AMBIENT AIR CONDITIONS ARE 1 BAR, 20°C, AND 60% RH.

The requirement is to **SATURATE INLET AIR AT CELL OPERATING TEMPERATURE OF 60°C**. Calculate the air flow rate, the amount of water required for 100% humidification of air at the inlet, and heat required for humidification.



Adopted from Frano Barbir

STEP #1:

WATER MASS FLOW RATE IN EXISTING INLET AIR ?

Air Flow Rate INLET @ 20C, 100 kPa

$$[\dot{m}_{air}]_{STACK} = S_{air} \frac{I}{4F} \frac{1}{0.21} = 2 \frac{0.6(A/cm^2) * 300(cm^2) * 100(plates)}{4 * 96,485 * 0.21} = 0.444 mol/s \cdot 28.85 g/mol = \frac{12.81 \text{ grams air/s}}{STACK}$$

Saturation Pressure @ 20C (293K)

$$p_{vs}(T) = e^C$$

$$C = aT^{-1} + b + cT + dT^2 + eT^3 + f \ln(T) \\ = 2.339 kPa$$

Mass Humidity Ratio @ 20C, 100 kPa

$$x = X \left[\frac{\text{moles vapor}}{\text{moles air}} \right] \cdot \frac{M_{H_2O}(g/mole)}{M_{air}(g/mole)} = \frac{\phi p_{vs}}{P_{TOTAL} - \phi p_{vs}} \cdot \frac{M_{H_2O}(g/mole)}{M_{air}(g/mole)} \\ = \frac{0.6 * 2.339}{100 - 0.6 * 2.339} \cdot \frac{18}{28.85} = 0.00888 \frac{\text{grams water vapor}}{\text{grams air}} = \text{mass humidity ratio}$$

$$\text{INLET AIR WATER} = 0.0088 \left[\frac{\text{grams water vapor}}{\text{grams air}} \right]$$

$$\dot{m}_{w@20C} = 12.81 \text{ grams air/s} \cdot 0.00888 \frac{\text{grams water}}{\text{grams air}} = 0.11 \text{ grams water/s}$$

$$x = \frac{\phi p_{vs}(T)}{P_{total} - \phi p_{vs}(T)} \cdot \frac{M_{H_2O}(g/mole)}{M_{air}(g/mole)}$$

STEP 2:

INJECTION WATER MASS FLOW RATE (@100%RH)

WATER INJECTION @ 60C, 115 kPa, RH 100%

Saturation Pressure @ 60C, 115kPa

$$p_{vs}(T) = e^C$$

$$C = aT^{-1} + b + cT + dT^2 + eT^3 + f \ln(T)$$
$$= 19.944 \text{ kPa}$$

Mass Humidity Ratio @ 60C

$$x = \frac{1.0 * 19.944 \text{ kPa}}{115 \text{ kPa} - 19.944 \text{ kPa}} \cdot \left[\frac{18}{28.85} \right] = 0.131 \frac{\text{grams water}}{\text{grams air}}$$

$$x = \frac{\phi p_{vs}(T)}{P_{total} - \phi p_{vs}(T)} \cdot \frac{M_{H_2O}(\text{g / mole})}{M_{air}(\text{g / mole})}$$

Finally

WATER in AIR @ 60C

$$m_{w@60C} = 12.81 \text{ grams air / s} * 0.131 \frac{\text{grams water}}{\text{grams air}} = 1.678 \text{ grams water / s}$$

Water Required for Humidification

$$m_w = 1.678 - 0.11 = 1.568 \text{ g / s}$$

IN GENERAL:

INLET WATER MASS FLOW RATE/CELL

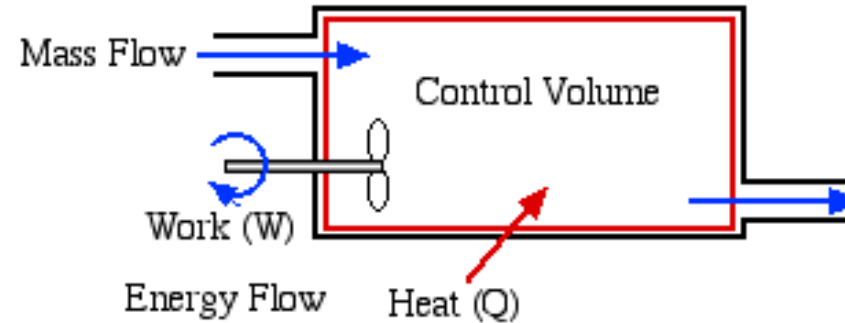
$$\dot{m}_{water_{IN}} = S_{air} \frac{I}{4F} \frac{1}{0.21} \left[\frac{mole}{sec} \right] \cdot MW_{air} \left[\frac{g}{mole} \right] \cdot \frac{\phi p_{vs}(T)}{P_{TOTAL} - \phi p_{vs}(T)} \left[\frac{mole\ vapor}{mole\ air} \right] \cdot \frac{M_{H_2O}(g/mole)}{M_{air}(g/mole)}$$

$$\dot{m}_{water_{IN}} = \left[\frac{\cancel{grams\ air}}{s} \right] \cdot \left[\frac{grams\ water\ vapor}{\cancel{grams\ air}} \right]$$

$$\dot{m}_{water_{IN}} \left[\frac{g\ water\ vapor}{s} \right] = \dot{m}_{Air_{IN}} \left[\frac{\cancel{grams\ air}}{s} \right] \cdot x \left[\frac{grams\ water\ vapor}{\cancel{grams\ air}} \right]$$

IN GENERAL

MASS CONSERVATION ENERGY CONSERVATION



Mass Conservation

$$\sum \dot{m}_{in} = \sum \dot{m}_{out}$$

$\dot{m} \rightarrow$ mass flow rate: kg/s

Energy Conservation

$$\sum \dot{Q}_{in} [W] + \sum \dot{m}_{in} h_{in} [W] = \sum \dot{m}_{out} h_{out} [W] + \sum \dot{Q}_{out} [W] + \dot{W}_{EL} [W]$$

$$h \rightarrow \left(cp \frac{J}{kg - C} \right) (T(C)) \rightarrow \text{enthalpy: J/kg}$$

$\dot{W}_{EL} \rightarrow$ Work Output Electrical

AIR/VAPOR ENTHALPY: THERMODYNAMICS

Enthalpy of Dry Gas (J/g)

$$h_g (J/g) = cp_g t$$

$$cp_g = \text{specific heat of dry gas} = J/g-K; \rightarrow cp_{AIR} = 1.01 J/g-K$$

t = temperature in C (reference state is 0 at 0C)

Enthalpy of Water Vapor (J/g)

$$h_v = cp_v t + h_{fg}; \rightarrow cp_{VAPOR} = 1.87 J/g-K$$

$$h_{fg} = \text{heat of evaporation} = 2500 J/g \text{ at } 0C$$

Enthalpy of Liquid Water (J/g)

$$h_w = cp_w t; \rightarrow cp_{WATER} = 4.18 J/g-K$$

Enthalpy of Humid Gas (J/g)

$$h_{vg} = cp_g t + x_v (cp_v t + h_{fg})$$

Enthalpy of Water Vapor and Liquid Water (J/g)

$$h_{vg} = cp_g t + x_v (cp_v t + h_{fg}) + x_w cp_w t$$

x_v = water vapor content (grams of vapor per gram of dry gas)

x_w = liquid water content (grams of liquid water per gram of dry gas)

$$x = x_v + x_w$$

Note: when $x_w = 0$, $x = x_v$; when $x_w > 0$, $x = x_{vs}$ (saturated)



HEAT CALCULATIONS (CHAPTER 5)

Enthlpy of Humid Gas (J/g)

$$h_{vg} = cp_g t + x_v (cp_v t + h_{fg}) \rightarrow t = 0^\circ C \rightarrow \text{Reference Zero State is a } 0^\circ C$$

$$h_{\text{amb air}} = 1.01J / g - K \cdot 20C + 0.00888 \cdot (1.87J / g - K \cdot 20C + 2500J / g) = 42.73J / g$$

$$\begin{aligned} H_{\text{AMB AIR}} &= h_{\text{amb air}} \cdot \dot{m}_{\text{air}} \\ &= 42.73J / g \cdot 12.81g / s = 546.9W \rightarrow \text{Energy Content} \end{aligned}$$

$$h_{\text{hum air}} = 1.01J / g - K \cdot 60C + 0.131 \cdot (1.87J / g - K \cdot 60C + 2500J / g) = 402.8J / g$$

$$\begin{aligned} H_{\text{HUM AIR}} &= h_{\text{hum air}} \cdot \dot{m}_{\text{air}} \\ &= 402.8J / g \cdot 12.81g / s = 5155.8W \rightarrow \text{Energy Content} \end{aligned}$$

$$\begin{aligned} h_{\text{water}} &= cp_w t \\ &= 4.18J / g - K \cdot 60C = 250J / g \end{aligned}$$

$$H_{\text{water}} = h_{\text{water}} \cdot 1.57g / s = 393.8W$$

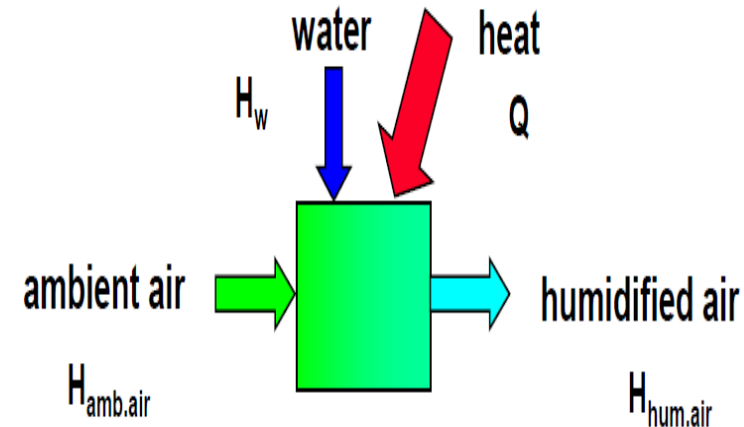
HEAT

$$\dot{E}_{in} - \dot{E}_{out} = 0$$

$$H_{\text{AMB AIR}} + H_{\text{water}} + Q = H_{\text{HUM AIR}}$$

$$\begin{aligned} Q &= H_{\text{HUM AIR}} - H_{\text{AMB AIR}} - H_{\text{water}} \\ &= 5155.8W - 546.9W - 393.8W \end{aligned}$$

$$= \frac{4215.1W}{\text{STACK}}$$



Heat needed from external source or from FUEL CELL STACK

EFFICIENCY AND WATER GENERATION

IN GENERAL

$$\begin{aligned} \text{Cell Power} &= \frac{\dot{W}_{elec}}{STACK} = I^* \left[\frac{Amps}{cm^2} \right] \cdot Area [cm^2] \cdot \frac{V}{cell} \cdot \#cells \\ &= 0.6 \left[\frac{Amps}{cm^2} \right] \cdot 300cm^2 \cdot 0.65 \frac{V}{cell} \cdot 100 \text{ cells} \\ &= 11,700 \text{ W} \end{aligned}$$

$$\text{Efficiency} = \eta = \frac{V / cell}{1.482} = 0.439$$

$$\begin{aligned} \text{Heat Generated} &= \frac{\dot{W}_{elec}}{\eta} - \dot{W}_{elec} \\ &= 14,951 \text{ Watts} \rightarrow \text{External Work and for Removal} \end{aligned}$$

$$\begin{aligned} \frac{\text{Water Generated}}{\text{Stack}} &= \frac{I^* \cdot Area}{2F} MW_{H_2O} \cdot \#cells \\ &= \frac{0.6 \cdot 300}{2 \cdot 96,485} \cdot 18 \cdot 100 \\ &= 1.68 \frac{g}{s} = 145.15 \frac{kg}{day} \cdot \frac{1L}{kg} = 145L / day \end{aligned}$$

$$\begin{aligned} P_{loss} &= q_{heat} = P_{max} - P_{actual} \\ &= \frac{1.482V}{cell} \cdot \frac{\#cells}{stack} \cdot I - \frac{V_{actual}}{cell} \frac{\#cells}{stack} \cdot I \end{aligned}$$

$$\frac{q_{heat}}{stack} = nI(1.482 - V_{cell_{average}}); \text{WATTS}$$

Heat generated from stack and to be dumped: 14.9kW.

Can this be used for HUMIDIFICATION at 4.2kW?

But do we have correct heat transfer driving temperature differential?
Can not transfer heat from LOW to HIGH. LTPEM FC have low grade heat.

SUMMARY-100 CELL STACK

$$POWER = 0.6 A / cm^2 * 300 cm^2 * 0.65 V / CELL * 100 CELLS = 11,700 W$$

$$EFF = 0.65 / 1.482 = 44\%$$

$$HEAT_{LOSS} = 11,700 / 0.44 - 11,700 = 14,951 W \rightarrow DISSIPATION$$

$$HEAT_{HUMID AIR} = 5155.8 W$$

$$HEAT_{AIR Ambient} = 402.8 W$$

$$HEAT_{WATER} = 393.8 W$$

$$WATER_{GEN} = 93 \cdot 10^{-6} \frac{g/s}{A-Cell} * (0.6 A / cm^2 * 300 cm^2 * 100 cells) = 1.679 g/s$$

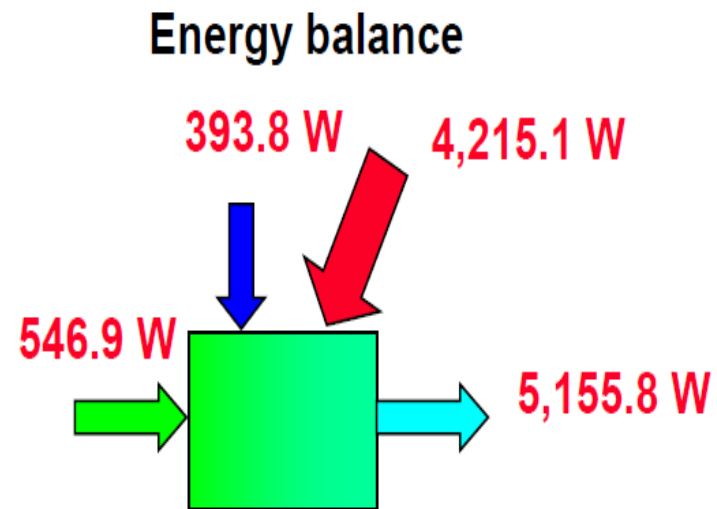
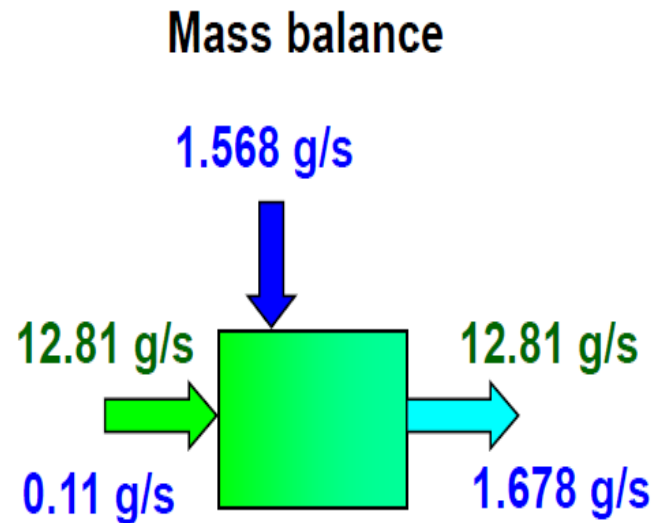
$$WATER_{AIR HUMD} = 1.568 g/s$$

CONSUMPTION RATES \rightarrow LIQUID PRODUCTS

$$\dot{m}_{H_2O} \left[\frac{g}{sec} \right] = \frac{I}{2F} \left[\frac{\text{moles of } H_2O \text{ Product}}{sec} \right] \cdot M_{W_{H_2O}} \left[\frac{g}{\text{moles of } H_2O} \right]$$

$$\dot{m} [SLM] = \frac{I}{nF} \left[\frac{\text{moles}}{sec} \right] \cdot M_{W_{H_2O}} \left[\frac{g}{mole} \right] \cdot \frac{60 sec}{min} \cdot \frac{1}{\rho_{H_2O} \frac{g}{m^3}} \cdot \frac{1000 L}{m^3}$$

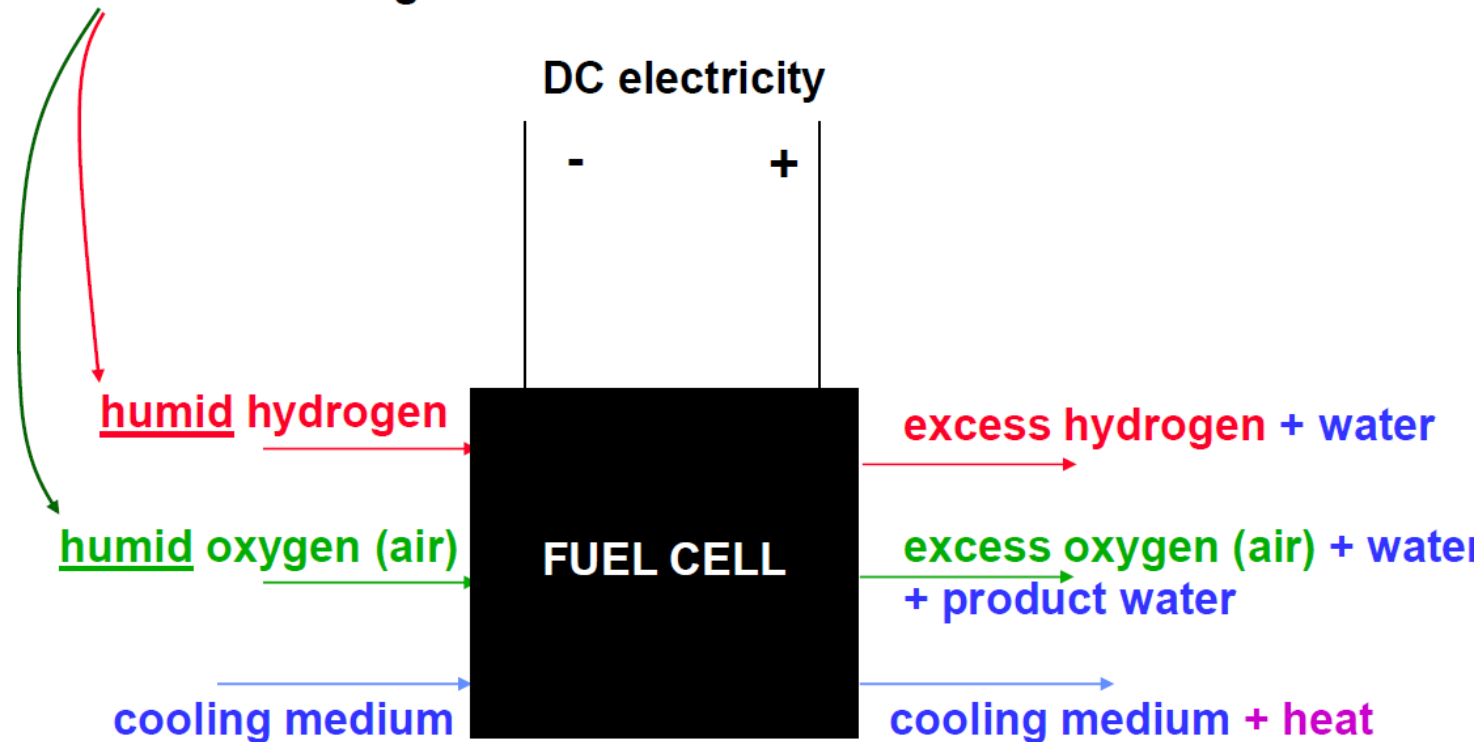
WATER MASS AND ENERGY BALANCE



Adopted from Frano Barbir

HUMIDIFICATION OF REACTANT GASSES

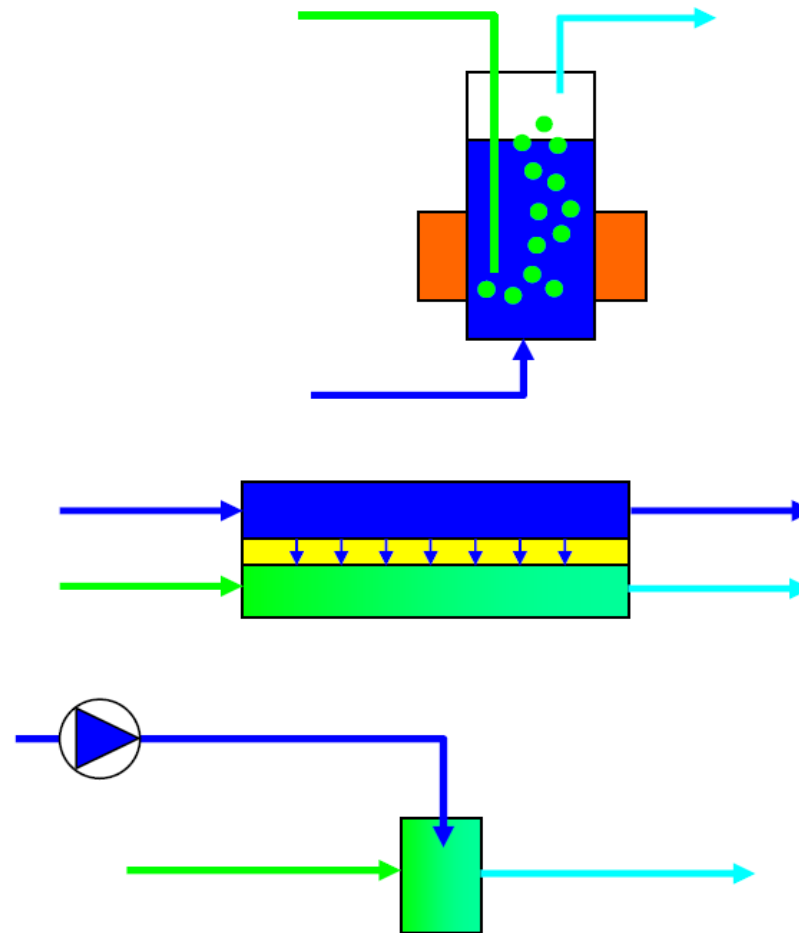
Typically both air (oxygen) and hydrogen must be humidified before entering the cell



Adopted from Frano Barbir

HUMIDIFICATION METHODS

- Bubbling
- Membrane
- Water injection
- Steam injection



Adopted from Frano Barbir

EXIT CONDITIONS

EXIT H2 MASS FLOW

$$\begin{aligned}\frac{\dot{m}_{H2out}}{cell} &= \dot{m}_{H2in} - \dot{m}_{H2CONSUMPTION} \\ &= S_{H_2} \frac{I}{2F} M_{H_2} - \frac{I}{2F} M_{H_2}, \rightarrow g / \text{sec} \\ &= (S_{H_2} - 1) \frac{I}{2F} M_{H_2} \text{ g/sec per cell}\end{aligned}$$

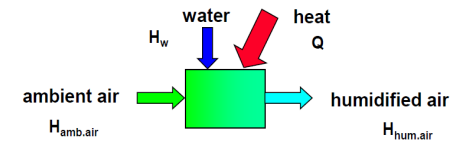
EXIT AIR/N2 MASS FLOW

$$\begin{aligned}\frac{\dot{m}_{AIRout}}{cell} &= \dot{m}_{O_2OUT} + \dot{m}_{N_2IN} \text{ (Nitrogen does not participate in the reaction)} \\ &= \left[(S_{O_2} - 1)M_{O_2} + S_{O_2} \frac{1 - r_{O_2in}}{r_{O_2in}} M_{N_2} \right] \frac{I}{4F} \text{ g/sec per cell}\end{aligned}$$

EXIT OXYGEN VOLUME FRACTION

$$r_{O_2out} = \frac{O_2_{OUT}}{AIR_{IN}} = \frac{S_{O_2} - 1}{\frac{S_{O_2}}{r_{O_2in}} - 1}; \quad r_{O_2in} = 0.21 \text{ Normally}$$

EXAMPLE 2



- 10kW H₂/Air FC operates at 0.7V/cell at TFC=70C, ambient pressure (101.3kPa), T₀=23C, RH=75%, and S_{o2}=2.25. How much water is needed for seven days of operation?

$$\phi = \text{Relative Humidity} = \frac{\text{"ACTUAL" vapor partial pressure}}{\text{vapor SATURATION pressure}} = \frac{p_v}{p_{vs}(T)}$$

Saturation Pressure @ 23C=296.15K

$$p_{vs}(T) = e^C; C = aT^{-1} + b + cT + dT^2 + eT^3 + f \ln(T)$$

$$p_{vs}(T = 23C) = 2.810 \text{ kPa}$$

Saturation Pressure @ 70C=343.15

$$p_{vs}(T = 70C) = 31.198 \text{ kPa}$$

Mass Humidity Ratio - Ambient (23C, RH=75%) ←

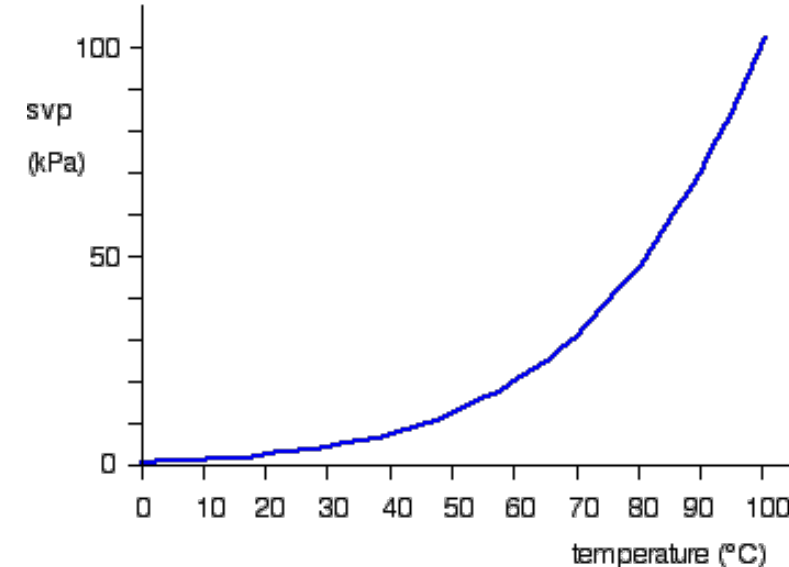
$$x = X \cdot \frac{M_{H_2O}(\text{g / mole})}{M_{air}(\text{g / mole})} = \frac{\phi p_{vs}}{P - \phi p_{vs}} \cdot \frac{M_{H_2O}(\text{g / mole})}{M_{air}(\text{g / mole})}$$

$$= \frac{18}{28.85} \frac{0.75 * 2.81}{101.3 - 0.75 * 2.81} = 0.01326 \frac{\text{grams water}}{\text{grams air}} = \text{mass humidity ratio}$$

Mass Humidity Ratio - Fuel Cell Inlet (70C, RH=100%) ←

$$= \frac{18}{28.85} \frac{1.0 * 31.198}{101.3 - 1.0 * 31.198} = 0.2776 \frac{\text{grams water}}{\text{grams air}} = \text{mass humidity ratio}$$

saturated vapour pressure of water



$$x \left[\frac{\text{grams } H_2O}{\text{grams Air}} \right] = \frac{\phi p_{vs}(T)}{P_{total} - \phi p_{vs}(T)} \cdot \frac{M_{H_2O}(\text{g / mole})}{M_{air}(\text{g / mole})}$$

Air Flow @ INPUT AMBIENT CONDITIONS

$$\frac{m_{air}}{cell} = S_{air} \frac{I}{4F} \frac{1}{0.21} \left[\frac{mole}{s} \right] M_{air} \left[\frac{g_{air}}{mole} \right] = 2.25 \frac{10000W \div 0.7V / cell}{4 \times 96,485} \frac{1}{0.21} 28.85; I = \frac{W}{V}$$

$$= 11.44 \frac{g_{air}}{sec} / cell$$

$$\dot{m}_{H_2O_{AIR}} \left[\frac{grams H_2O}{s} \right] = \dot{m}_{AIR} \left[\frac{grams Air}{s} \right] \cdot x \left[\frac{grams H_2O}{grams Air} \right]$$

Water in Air INPUT(23C,75RH)

$$m_{wairINPUT} = 11.44 \frac{g_{air}}{sec} / cell \cdot 0.01326 \frac{grams water}{grams air} = 0.1516 \frac{grams water}{sec} / cell$$

Water Generated

$$m_{wgen} = \frac{I}{2F} M_{H_2O} = 1.333 \frac{g}{s} / cell \text{ (eqn.5-7)}$$

Water at Fuel Cell Outlet "AIR"

$$m_{wout} = m_{wairINPUT} + m_{wgen} = (0.1516 + 1.333) = 1.4846 \frac{grams water}{sec} / cell \rightarrow \text{WATER OUT}$$

AIR OUT FLOW RATE

$$m_{AirOut} = 10.27976 \frac{g_{air}}{s} / cell \text{ (eqn.5-68)} \rightarrow \text{DEPLETED AIR FLOW OUT}$$

Mass Hummidity Ratio at Outlet

$$x_{OUTLET} = \frac{grams water}{grams air} = \frac{m_{wout}}{m_{AirOut}} = \frac{1.4846 \frac{grams water}{sec} / cell}{10.27976 \frac{g_{air}}{s} / cell} = 0.14456 \frac{grams water}{grams air}$$

For 100% Humidity at Exit, We Need

$$[m_{H_2O}]_{OUT} = 10.27976 \frac{g_{air}}{s} / cell \cdot (0.2776 - 0.14456) \frac{grams water}{grams air} = 1.3676 \frac{grams water}{sec} / cell$$

$$m_{H_2O_{7-DAYS}} = 1.3676 \frac{grams water}{sec} / cell \cdot \frac{3600sec}{hr} \cdot \frac{24hr}{Days} \cdot 7Days = 827kg \cdot \frac{m^3}{1000kg} \cdot \frac{1000L}{m^3} = 827 \frac{Liters}{cell}$$

Fuel cell generates 100 amps at 0.6V. H₂ flow is 1.8 NL/m,
 Air flow is 8.9 NL/m. Find
 a. H₂ Stoic; b. O₂ Stoic, c. O₂ at Outlet

Problem 5.1					
I	100	Amps			
V _{cell}	0.6	V			
q _{dot} H ₂ _in	1.8	NL/min			
q _{dot} Air_in	8.9	Ni/min			
rho_H2	0.090	kg/m ³	(g/l)	from P = rhoRT	
rho_Air	1.287	kg/m ³	(g/l)		
m _{dot} H ₂ _in	0.0027	g/s			
m _{dot} Air_in	0.1909	g/s			
S_H2	2.58			from Eq. 5-50	
S_O2	5.36			from Eq. 5-53	
c_O2_out	0.1778			from Eq. 5-17	